Possible Causes of Three-Dimensional Structural Deviations in the Neighborhood of Cranial Landmarks: Occlusal Force and Aging

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Abstract To seek the causes of three-dimensional morphological variations in the human skull, correlations between the 3D structural deviations in the neighborhood of cranial landmarks obtained by the finite element scaling method and the degree of dental wear or age were examined by principal component analysis using three male adult samples from Japanese, Indians, and African-Americans. The results showed that the degree of dental wear is positively associated with the magnitude of strain at the inion in Japanese; that dental wear is inversely associated with the magnitude of strain at the frontotemporale in Japanese; and that age is positively associated with the magnitude of strain at the center of the parietal tuber in African-Americans. These significant associations suggest, at least, that the craniofacial form varies along with age even in adulthood and, possibly, also in response to mechanical stresses from the masticatory and/or nuchal muscles. **Key words :** Human cranial form, Three-dimensional coordinates, Finite element scaling analysis, Dental wear, Age

In recent years, with the development of apparatus and software for capturing and analyzing three-dimensional (3D) coordinates, many geometric morphometric (Marcus et al., 1996) studies have been carried out in the field of physical anthropology. Although most of them were based on the generalized Procrustes analysis (e.g., Detroit, 2000; Bookstein, 1991; Hennessy and Stringer, 2002; Bookstein et al., 2003; Harvati, 2003; Slice, 2005; Gunz and Harvati, 2007; Gunz et al., 2009; Hublin et al., 2009; Makishima and Ogihara, 2009; Bigoni et al., 2010; Fukumoto and Kondo, 2010; Harvati et al., 2010; Neubauer et al., 2010; Williams and Slice, 2010; Bienvenu et al., 2011; Coquerelle et al., 2011; Gonzalez et al., 2011; Noback et al., 2011; von Cramon-Taubadel, 2011; Weisensee and Jantz, 2011; Freidline et al., 2012; Singh et al., 2012; von Cramon-Taubadel and Smith, 2012), there is another useful method to quantify the magnitude and direction of strain at an arbitrary point of a 3D form in the change from the form to another corresponding form. This method is the finite element scaling method (FESM). This was developed by Lewis *et al.* (1980), Cheverud *et al.* (1983), and their colleagues in the 1980s and has been used by several researchers (Cheverud and Richtsmeier, 1986; Richtsmeier, 1987; Mine and Ogata, 1989; Cheverud *et al.*, 1992; Kohn *et al.*, 1993, 1995; Richtsmeier and Walker, 1993; Mizoguchi, 2000a, b, 2005; Matsukawa, 2002). Both methods are useful for the analysis of form and have many similar strong points. However, one of the major differences between them is that, in generalized Procrustes analysis (GPA), original configurations are standardized by the centroid size, while in finite element scaling analysis (FESA), size is not removed.

In the present study, using the FESM, it is examined whether or not there are any associations between 3D structural deviations in the neighborhood of some cranial landmarks and the degree of occlusal wear on the maxillary first molar (UM1) or age, in order to explore the possibility that masticatory force and/or aging are causes of part of the morphological variation in the human skull.

Materials and Methods

Three male adult samples were used. One consists of 37 skulls of Japanese from the end of the early modern "Edo" period (A.D. 1603 to 1867). These are stored in the University Museum, the University of Tokyo, Japan. The second sample is composed of 30 skulls of African-Americans randomly extracted from the Terry Collection housed in the National Museum of Natural History, Smithsonian Institution, Washington, D.C., U.S.A. They died during the period of 1926 to 1944, and the age-at-death ranges from 21 to 68. The final one is a sample of 35 Indian skulls, which are stored in Nihon University School of Dentistry at Matsudo, Chiba, Japan.

Age-at-death is known for individual specimens of the Terry Collection. For the other two samples, however, there are no such records. Therefore, the degree of occlusal wear on the UM1 was recorded as an indicator of age according to Broca's grading system (Martin and Saller, 1957). It is to be regretted, however, that the present author did not record the degree of dental wear for the sample from the Terry Collection because he did not intend to analyze the relationship between occlusal force and age at that time. Erasing the effect of aging from dental wear is a future task.

All 3D coordinates for cranial landmarks were obtained by the present author on the basis of trigonometric measurements using sliding and spreading calipers. The Japanese skulls were measured twice to assess intra-observer errors during the periods of September, 1976, to January, 1977, and September, 1977, to December, 1977; the African-American skulls, in April and May, 1987; and the Indian skulls, between April, 1994, and October, 1996. Basically, the coordinates of a landmark are calculated using the line segments between the landmark and three of the following five landmarks: nasion, bregma, lambda, right asterion, and left asterion. In the present study, the positive direction of the *x*-axis

or anterior-posterior axis of the skull points to the anterior side; that of the *y*-axis or medial-lateral axis points to the left; and that of the *z*-axis or superior-inferior axis points to the superior.

The practical objects analyzed by FESM are six elements or hexahedra set in the cranium (Fig. 1). The eight nodes of each hexahedron are as follows.

- Right element 1 (anterior neurocranium): nasion (n), grabella (g), bregma (b), basion (ba), right frontotemporale (ft), the center of the right frontal tuber (STH), right eurion (eu), and right porion (po)
- Left element 1 (anterior neurocranium): n, g,
 b, ba, left ft, left STH, left eu, and left po
- Right element 2 (posterior neurocranium): b, ba, inion (i), lambda (l), right eu, right po, right asterion (ast), and the center of the right parietal tuber (SCH)
- 4) Left element 2 (posterior neurocranium): b, ba, i, l, left eu, left po, left ast, and left SCH
- 5) Right element 3 (orbito-zygomatic region): g, right frontomalare temporale (fmt), right po, opisthion (o), n, right orbitale (or), right zygomaxillare (zm), and ba
- 6) Left element 3 (orbito-zygomatic region): g, left fmt, left po, o, n, left or, left zm, and ba

The definitions of the above landmarks except for STH and SCH can be found in Martin and Saller (1957). STH was marked with a pencil by viewing from superior and lateral directions, and SCH, from superior and posterior directions. This method may be somewhat subjective.

For each node of the six hexahedra, the magnitude of 3D structural deviation (from the 'mean' cranium in each sample) called 'principal value' and its direction cosines were first estimated by FESM. The details of the FESM and the relevant procedures are described in Lewis *et al.* (1980), Cheverud *et al.* (1983), Cheverud and Richtsmeier (1986), Leigh and Cheverud (1991), Cheverud *et al.* (1992), Malvern (1969), Bathe and Wilson (1976), and Mizoguchi (2000b). In the present study, principal values were linear-



Fig. 1. Elements set up in the cranium and the cranial landmarks used. **a.** Bird's-eye view. **b.** Anterior view. **c.** Lateral view. **d.** Inferior view.

ized using the following formula (Cheverud and Richtsmeier, 1986; Cheverud *et al.*, 1992) before use in multivariate analyses:

$$L_i = \ln \left[(1 + 2P_i)^{1/2} \right]_i$$

where P_i is the *i*-th principal value (i = 1, 2, and 3), and L_i is the value transformed to a linear or additive scale.

The intra-observer errors for linearized principal values and direction cosines were evaluated by the double determination method (Lundström, 1948; Mizoguchi, 1977). To check the relative magnitude of errors, intraclass correlation coefficients (Cavalli-Sforza and Bodmer, 1971) were calculated between the duplicate data sets of the early modern Japanese sample.

To examine the overall or local relationships between 3D structural strains and dental wear or age, principal component analysis, often abbreviated to PCA, (Lawley and Maxwell, 1963; Okuno *et al.*, 1971, 1976; Takeuchi and Yanai, 1972) was applied to the correlation matrices. The correlations between age and the principal values and direction cosines were estimated using Pearson's product-moment correlation coefficient, and those between such 3D variables and the degree of occlusal wear on the UM1 were estimated using four-fold point correlation coefficient (Yasuda, 1969).

At this step, however, only six nodes were selected for a set of three elements on one side because of the statistical limitation on the number of variables and sample size. In practice, one set of six nodes was chosen from the viewpoint of a possible relationship with the degree of development of skeletal muscles or growth: ft, STH, i, SCH, g, and zm; and the other set mainly contains intersections of sutures: b, ba, l, ast, fmt, and n.

The number of principal components was determined so that the cumulative proportion of the variances of the principal components exceeded 80%. The principal components obtained were then transformed by Kaiser's normal varimax rotation method (Asano, 1971; Okuno *et al.*, 1971) into different factors in an attempt to reveal other associations behind the variables.

The significance of factor loadings was tested by the bootstrap method (Efron, 1979a, b, 1982; Diaconis and Efron, 1983; Mizoguchi, 1993). In order to estimate the bootstrap standard deviation of a factor loading, 1,000 bootstrap replications, including the observed sample, were used. The bootstrap standard deviation was estimated by directly counting the cumulative frequency for the standard deviation in the bootstrap distribution.

The presence of common factors, such as those represented by principal components (PCs) or rotated factors (Facs), was further tested by evaluating the similarities between the factors obtained for the three samples, namely, by estimating Kendall's rank correlation coefficient, tau (Siegel, 1956), between the patterns of variation of factor loadings. It should be noted here that a certain common factor (PC in practice) extracted from the PCA for a certain sample can be detected as a rotated factor in the rotated solution of the PCs extracted from another similar sample, as shown in Mizoguchi (2004). Therefore, PCs and Facs are equivalently treated in this study.

Mathematical and statistical calculations were executed using programs written by the author in FORTRAN: THRCR3 for calculating 3D coordinates of cranial landmarks, FESM for finite element scaling analysis, MIVCRL for intraclass correlation coefficients, BTPCA for principal component analysis and Kaiser's normal varimax rotation, and RKCNCT for rank correlation coefficients. The FORTRAN 77 compiler used is FTN77 for personal computers, provided by Salford Software Ltd. To increase efficiency during programming and calculation, a GUI for programming, CPad, provided by "kito," was used. 3D illustrations of the human skull were drawn by the present author with Rokkaku-Daiou Super 6 (Ver. 6.3.1) of CELSYS, Inc., utilizing a free 3D model, "Skull N070211-3D model," created by Fahim Fazli as a template.

Results

Intraclass correlations between the duplicate data sets from the early modern Japanese sample are shown in Table 1. The intraclass correlation coefficients independently obtained from the right and left sides reveal at least two similar tendencies. One is that the intra-observer errors on the principal values tend to be lower than those on the corresponding direction cosines in most of the landmarks examined. The other is that, against our expectation, while the intraclass correlation coefficients on the nasion and glabella are extremely low, those on the inion and SCH are relatively high. Such a difference may be partly caused by the use of different sets of three landmarks on which the determination of the coordinates of landmarks in question is based. In any case, the results of the following analyses, especially on the nasion and glabella, must be carefully interpreted.

In Tables 2 to 13, the factor loadings on PCs

Variable ²	Right	Left	Variable ²	Right	Left
Element 1 (Anterior neurocranium))		Element 2 (Posterior neurocran	ium)	
Node 1 (n): 1st p.v.	0.17	0.23	Node 6 (po): 1st p.v.	0.85***	0.81***
a-p	0.40**	0.64***	a-p	0.65***	0.58***
m–l	0.05	0.13	m—l	0.83***	0.51***
s—i	0.68***	0.32*	s—i	0.70***	0.59***
Node 2 (g): 1st p.v.	0.17	0.20	Node 7 (ast): 1st p.v.	0.83***	0.63***
a-p	0.47**	0.35*	a-p	0.86***	0.52***
m–l	-0.10^{3}	0.56***	m—l	0.54***	0.62***
s—i	0.37*	0.40**	s—i	0.70***	0.71***
Node 3 (b): 1st $p.y$.	0.91***	0.90***	Node 8 (SCH): 1st p.v.	0.85***	0.89***
a=p	0.28*	0.66***	a–p	0.54***	0.76***
m_l	0.41**	0.28*	m_l	0.42**	0.53***
s=i	0.52***	0.68***	s—i	0.45**	0.50***
Node 4 (ba): 1st p v	0.75***	0 78***	Centroid: 1st p v	0.87***	0.90***
a_n	0.72***	0.84***	a–n	0.85***	0.68***
m_l	0.71***	0.39**	m_l	0.86***	0.47**
5_i	0.68***	0.71***	s_i	0.85***	0.68***
Node 5 (ft): 1st n v	0.80***	0.82***	Element 3 (Orbito-zygomatic r	egion)	0.00
a_n	0.43**	0.61***	Node 1 (g): 1st n v	0.25	0.26
u p m_l	0.43**	0.57***	a_n	0.43**	0.51***
	0.45	0.50***	a-p m l	0.45	0.00
Node 6 (STH): 1st n v	0.55***	0.50	111-1 s_i	0.54	0.00
	0.43**	0.34*	Node 2 (fmt): 1st n v	0.50***	0.46**
a-p m l	0.45	0.24	Node 2 (mit). 1st p.v.	0.39	0.40
III-I a i	0.43	0.20	a–p	0.22	0.51
S-I Nodo 7 (au): 1st p v	0.07	0.40		0.57	0.50
Node / (eu). 1st p.v.	0.91	0.69	S-I Noda 2 (no): 1st n v	0.35	0.33
a-p	0.75	0.47	Node 5 (po). 1st p.v.	0.70	0.70
III—I - :	0.33	0.50	a-p	0.72	0.00
S=1	0.01	0.30	m–1	0.70	0.19
Node 8 (po): 1st p.v.	0.88	0.80	S=1	0.75	0.27
a–p	0.55	0.90	Node 4 (0): 1st p.v.	0.79	0.84
m—i	0.04	0.85	a–p	0.01	0.43
S-1	0.41	0.85	m—I	0.19	0.23
Centroid: 1st p.v.	0.95	0.94	S-1	0.68	0.58
a-p	0.66	0.51	Node 5 (n): 1st p.v.	0.30	0.09
m—l	0.68***	0.37*	a-p	0.64	0.14
S-1	0.71***	0.63	m–l	0.34*	0.02
Element 2 (Posterior neurocranium)	* * *	S-1	0.55***	0.47**
Node 1 (b): 1st p.v.	0.95	0.93	Node 6 (or): 1st p.v.	0.66	0.74***
a-p	0.71***	0.73***	a-p	0.78***	0.42**
m–l	0.68***	0.36*	m—l	0.66***	0.43**
S—1	0.62***	0.41**	s—i	0.55***	0.21
Node 2 (ba): 1st p.v.	0.68***	0.85***	Node 7 (zm): 1st p.v.	0.79***	0.76***
a–p	0.68***	0.37*	a–p	0.31*	0.45**
m—l	0.43**	0.39**	m—l	0.40**	0.62***
s—i	0.60***	0.71***	s—i	0.72***	0.49**
Node 3 (i): 1st p.v.	0.97***	0.92***	Node 8 (ba): 1st p.v.	0.82***	0.69***
a–p	0.89***	0.60***	a–p	0.45**	0.57***
m—l	0.81***	0.67***	m—l	0.47**	0.56***
s—i	0.97***	0.92***	s—i	0.42**	0.70***
Node 4 (l): 1st p.v.	0.95***	0.96***	Centroid: 1st p.v.	0.67***	0.80^{***}
a–p	0.75***	0.74***	a-p	0.81***	0.75***
m_l	0.86***	0.61***	m_l	0.68***	0.46**
s—i	0.73***	0.55***	s—i	0.75***	0.57***
Node 5 (eu): 1st p.v.	0.65***	0.80***			
a–p	0.58***	0.79***			

Table 1. Intraclass correlation coefficients between the first and second data sets from early modern Japanese in the linearized first principal values and their direction cosines at the eight nodes and centroid of each of six regional elements (hexahedra) of the skull.¹

¹The sample size (i.e., no. of pairs) is 32.

а–р

m–l

s—i

²p.v.: principal value; a–p: direction cosine for the anterior-posterior axis; m–l: direction cosine for the medial-lateral axis; s-i: direction cosine for the superior-inferior axis.

0.36*

0.59***

³ Underestimate due to a sampling error. *P < 0.05; **P < 0.01; ***P < 0.001, by a one-tailed test.

0.33*

0.36*

and rotated factors for ft, STH, i, SCH, g, and zm are listed, and, in Tables 14 to 25, those for b, ba, l, ast, fmt, and n are shown. Remarkable findings are as follows.

First, both PC IV from the right elements (Table 2) and PC VIII from the left elements (Table 4) of early modern Japanese have highly significant correlations (P < 0.001) with the degree of dental wear and the first principal value at the inion (Fig. 2). Furthermore, both PC VIIIs from the right and left elements (Tables 2 and 4) have highly significant positive correlations (P < 0.001) with dental wear and inverse correlations (P < 0.001) with the first principal value at the front otemporale.

Not only Fac II from the right elements (Table 11) but also Fac IX from the left elements (Table 13) of African-Americans reveals that age is significantly associated with the principal value at SCH (P < 0.01). This association is confirmed by the significant rank correlation coefficient of 0.53 (P < 0.001) between these factors in the pattern of variation of factor loadings (Table 26).

Both PC IV from the right elements (Table 14) and PC VIII from the left elements (Table 16) of early modern Japanese show that the degree of dental wear is positively associated with the principal value at the frontomalare temporale (P < 0.01) and inversely associated with the principal value at the asterion (P < 0.001).

In the data set of Indians, however, no consistent tendency was found with respect to the associations between dental wear and 3D structural deviations at landmarks.

Discussion

To date, several FESAs of the human skull have been conducted. For example, Cheverud *et al.* (1992) and Kohn *et al.* (1993, 1995) examined the effect of artificial cranial vault deformation on the cranial base and face using Native American samples; Richtsmeier (1987) studied morphological differences between the craniofacial complex of normal individuals and those affected with the syndromes of Apert and Crouzon; and Richtsmeier and Walker (1993) extracted properties of the facial skeleton of a juvenile *Homo erectus* from Nariokotome, Kenya, by comparison with the faces of some modern humans, chimpanzees, and simulated *Homo erectus* individuals. To the best of the present author's knowledge, however, there have been no FESAs on the associations of cranial landmarks with dental wear, except for those by Mizoguchi (2000a, 2005).

Associations with dental wear or age

Mizoguchi (2000a), using the same sample from early modern Japanese as used here, carried out FESAs of three neurocranial elements, which were however different from those examined in the present study, and showed that the local shape differences (the so-called standard deviation of transformed principal value) at left frontomalare temporale and left orbitale were inversely correlated with the degree of occlusal wear on the UM1. This implies that those individuals who have weaker dental wear tend to have a more distorted face in the regions near the temporalis muscle.

Furthermore, Mizoguchi (2005), using the same sample and the same neurocranial elements as in his previous work (2000a), revealed that the neurocranium of a person having heavily worn molars tended to be flatter and broader in its anterior-superior part (left STH and right and left ft) and narrower and higher in its posterior-inferior part (right ast and right and left po). He considered that this result suggests that the neurocranial form may partly be determined or modified by the development of the masticatory muscles that produce dental wear. It should be noted in his analyses, however, that, while dental wear was associated with the direction of 3D deviations, it was not so strongly related with their magnitude.

In the present study, a different set of elements from that used by Mizoguchi (2000a, 2005) was examined. Although Mizoguchi (2000a, 2005) dealt with only a limited part of the face, the present study was conducted on a slightly

variance PC1 II IV V VI VII VII IX X Y Y VI VII VII IX X Y Y VI VII VII IX X Y Y Y VII VII IX X Y Y Y VI VII VII VII X Y Y Y Y Y VI VII VII Y	· · · · · · · · · · · · · · · · · · ·	0				Ľ	actor loading	s					Total
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	variable	PC I	Π	III	IV	Λ	IV	IIV	IIIA	IX	Х	IX	variance (%)
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Node 5 (ft) of Element 1: 1st p.v.	0.10	0.48***	0.50***	-0.01	0.32***	0.02	0.26^{***}	-0.15^{***}	0.04	0.15***	0.25***	77.25
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	a-p m-l	-0.54*** -0.03	- 0.00 - 0.04	0.03	-0.55 0.34	-0.30	-0.16 -0.39	-0.32 0.57^{*}	-0.19	-0.01	-0.10 -0.20	-0.10	87.79 87.94
Node 6 (STH) of Element 1: 1st p.v. 0.064** 0.01 0.39*** 0.27** 0.21*** -0.22*** -0.04 0.17*** 0.2 0.03 0.03 0.037 0.03 0.043*** 0.056*** 0.01 0.035 0.04 0.16 0.01 0.037 0.03 0.037 0.03 0.043**** 0.025 0.04 0.16 0.01 0.01 0.043 0.18************************************	s-i	0.55***	-0.08	-0.56	0.29	- 0.08	0.30	0.11	0.01	-0.18	0.13	0.14	87.80
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Node 6 (STH) of Element 1: 1st p.v.	0.64** 0.56***	-0.51	0.39^{***}	0.27^{***}	0.21***	-0.22^{***}	-0.04 -0.18	0.18^{***} - 0.05	-0.04	0.17^{***} - 0.16	0.20^{***}	83.14 77 10
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	m_l	-0.56^{***}	0.16	-0.26	0.21	0.09	-0.37	0.09	0.43^{*}	-0.25	0.02	0.03	85.23
Node 3 (1) of Element 2: 1st p.v. -0.46 , -0.02 , -0.03 , -0.18 , 0.13 , 0.13 , 0.13 , 0.13 , 0.12 , -0.22 , -0.12 , 0.13 , 0.13 , 0.13 , 0.13 , 0.13 , 0.13 , 0.12	S-i S C C C C C C C C C C C C C C C C C C	-0.06	0.44	0.24	-0.22	-0.21	0.43	0.44	-0.06	0.18	0.23	-0.29^{*}	90.02
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	Node 3 (1) 01 Element 2: 15t p.v. a-n	- 0.40 0.63***	-0.40	-0.03	-0.18	0.15	0.14	0.27	- 07.0 -	-0.12	-0.22	-0.04	/4.22 84 65
Node 8 (SCH) of Element 2: 1st p.v. $-0.64^{***} -0.25$ -0.13 -0.20 -0.36 $0.069^{***} -0.08$ -0.05 0.19 0.07 0.07 0.10 0.07 0.01 0.010 0.01 0.017 0.010 0.07 -0.05 0.01 0.07 0.07 0.01 0.017 0.018 -0.017 0.012 0.014 0.05 0.018 -0.012 0.011 0.07 -0.011 0.017 0.022 0.04 0.05 0.018 0.012 0.011 0.017 0.012	m—l	0.10	0.34	0.06	0.46	0.15	-0.22	-0.47	-0.16	0.23	0.24	0.00	76.14
Node 8 (SCH) of Element 2: Isp.v. 0.19 -0.13 0.03 0.03 0.04 0.10 0.17 0.11 0.02 0.01 0.07 -0.03 0.01 0.17 0.11 0.02 0.01 0.07 -0.01 0.07 -0.01 0.07 0.01 0.17 0.11 0.02 0.02 0.01 0.07 -0.01 0.07 -0.01 0.07 0.01 0.07 -0.01 0.07 0.01 0.07 -0.01 0.07 0.01 0.07 -0.01 0.07 0.02 0.04 0.05 0.01 0.07 -0.01 0.07 -0.01 0.07 0.02 0.04 0.05 0.01 0.00 -0.028 0.04 0.05 0.01 0.00 -0.018 0.02 0.02 0.04 0.07 0.018 0.01 0.07 -0.01 0.07 0.018 0.01 0.00 -0.08 0.02 -0.017 0.02 0.018 0.01 0.018 0.01 0.02 0.02 0.01 0.02 0.018 0.01 0.018 0.012 0.018 0.02 0.02 0.018 0.012 0.012 0.018 0.012 0.018 0.012 0.010 0.018 0.012 0.010 0.018 0.012 0.010 0.022 0.011 0.007 0.020 0.011 0.007 0.000 0.018 0.012 0.010 0.022 0.017 0.000 0.018 0.012 0.010 0.022 0.017 0.000 0.022 0.017 0.000 0.022 0.017 0.000 0.022 0.017 0.000 0.022 0.017 0.002 0.012 0.017 0.020 0.012 0.017 0.020 0.012 0.017 0.002 0.012 0.017 0.020 0.012 0.017 0.020 0.012	S-i-S	-0.64^{***}	-0.25	-0.13	-0.20	-0.36	0.05	-0.08	-0.05	0.19	0.07	0.40^{***}	88.07
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Node 8 (SCH) of Element 2: 1st p.v.	0.19	-0.13	0.03	0.03	0.69***	-0.48**	0.18	-0.16	0.10	- 0.05	- 0.04	83.34
Node I (g) of Element 3: 1st p.v. -0.33 0.45 -0.18 0.22 0.28 0.02 0.04 0.05 0.08 0.11 0.02 0.02 0.03 0.08 0.11 0.00 0.02 0.02 0.03 0.08 0.01 0.00 0.02 0.03 0.08 0.01 0.00 0.02 0.03 0.08 0.01 0.00 0.02 0.00 0.02 0.00 0.00 0.00	a-p m-l	-0.028	-010 010	-0.40 -0.17	0.40	0.10	0.17	-0.23	c0.0 0 02	- 0.01 0.24	0.07	0.11	71.87
Node 1 (g) of Element 3: 1st p.v. -0.33 0.64*** 0.09 -0.15 -0.11 -0.22** -0.15* 0.04 -0.07 -0.038*** -0.0 are -0.08 -0.03 -0.03 -0.03 -0.13 0.00 -0.08 -0.03 -0.13 0.00 -0.08 -0.13 -0.00 0.08 -0.13 s.1 -0.06 -0.05 -0.05 -0.05 -0.05 -0.012 -0.07 -0.03 -0.02 -0.07 -0.02 -0.07 -0.03 -0.02 -0.07 -0.03 -0.02 -0.07 -0.03 -0.02 -0.07 -0.02 -0.05 -0.02 -0.03 -0.02 -0.03 -0.03 -0.03 -0.03 -0.03 -0.02 -0.07 -0.02 -0.07 -0.02 -0.	S-1	0.52***	-0.33	0.45	-0.18	-0.28	-0.28	0.02	0.04	0.05	0.08	0.19	81.84
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Node 1 (g) of Element 3: 1st p.v.	-0.33	0.64^{***}	0.09	-0.15	-0.11	-0.22^{**}	-0.15^{*}	0.04	-0.07	-0.33^{***}	-0.01	74.66
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	a-p	-0.08	-0.82^{***}	-0.13	0.13	0.00	-0.08	0.02	-0.17	0.00	0.08	-0.12	77.93
Node 7 (zm) of Element 3: 1st p.v. -0.22 -0.01 $-0.38**$ 0.19^{**} $0.11**$ 0.20 -0.05 -0.02 -0.05 -0.05 -0.05 -0.05 -0.12^{***} 0.20 0.15^{***} 0.20 0.15^{***} 0.22^{**} 0.12^{**} $0.12^$	m-l	-0.06	- 0.05	0.51	0.12	0.25	0.21	-0.23	0.48*	0.32	- 0.00	-0.28°	85.88
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	S—1 Node 7 (zm) of Flement 3· 1st n v	-0.20	-0.02 -0.14^{***}	- 0.30 0.38***	-0.14 0.19***	0.32***	-0.00 0.40***	- 0.07 - 0.07	- 0.02	-0.0/ -0.15^{***}	-0.20	0.14	03.41 03.41
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		0.33°	0.31	-0.48	-0.31	0.03	-0.02	-0.05	0.07	0.50^{**}	-0.26	0.24*	92.08
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	m_l	-0.62^{***}	-0.23	0.09	-0.02	0.35	-0.15	0.27	-0.08	-0.24	0.12	0.07	74.32
$ \begin{array}{cccc} \text{Occlusal wear of UM1} & 0.09 & -0.08 & -0.07 & -0.57^{***} & 0.07 & 0.10 & -0.21 & 0.55^{***} & -0.14 & 0.34^{*} & 0.27 \\ \text{Total corribution (%)} & 17.03 & 12.09 & 9.95 & 8.46 & 7.77 & 6.54 & 2.79 & 4.51 & 3.89 & 3.59 & 3.57 \\ \text{Cumulative removing (%)} & 17.03 & 2912 & 3907 & 4753 & 553.00 & 61.85 & 67.64 & 72.15 & 76.04 & 79.63 & 32.24 \\ \text{Cumulative removing (%)} & 17.03 & 2912 & 3907 & 4753 & 553.00 & 61.85 & 67.64 & 72.15 & 76.04 & 79.63 & 32.24 \\ \text{Cumulative removing (%)} & 17.03 & 2912 & 3907 & 4753 & 553.00 & 61.85 & 67.64 & 72.15 & 76.04 & 79.63 & 32.24 \\ \text{Cumulative removing (%)} & 17.03 & 2912 & 3907 & 4753 & 553.00 & 61.85 & 67.64 & 72.15 & 76.04 \\ \text{Cumulative removing (%)} & 17.03 & 2912 & 3907 & 4753 & 553.00 & 61.85 & 67.64 & 72.15 & 76.04 \\ \text{Cumulative removing (%)} & 17.03 & 2912 & 3907 & 4753 & 553.00 & 61.85 & 67.64 & 72.15 & 76.04 \\ \text{Cumulative removing (%)} & 17.03 & 2912 & 3907 & 4753 & 553.00 & 61.85 & 67.64 & 72.15 & 76.04 \\ \text{Cumulative removing (%)} & 17.03 & 2912 & 3907 & 4753 & 553.00 & 61.85 & 67.64 & 72.15 & 76.04 \\ \text{Cumulative removing (%)} & 17.03 & 2912 & 3907 & 4753 & 553.00 & 61.85 & 67.64 & 72.15 & 76.04 \\ \text{Cumulative removing (%)} & 17.03 & 2912 & 3907 & 4753 & 553.00 & 61.85 & 67.64 & 72.15 & 76.04 \\ \text{Cumulative removing (%)} & 17.03 & 2912 & 3907 & 4753 & 553.00 & 61.85 & 67.64 & 72.15 & 76.04 \\ \text{Cumulative removing (%)} & 17.03 & 57.04 & 57.04 & 57.04 & 57.04 \\ \text{Cumulative removing (%)} & 17.03 & 57.04 & 57.04 & 57.04 & 57.04 \\ \text{Cumulative removing (%)} & 17.03 & 57.04 & 57.04 & 57.04 & 57.04 \\ \text{Cumulative removing (%)} & 17.03 & 57.04 & 57.04 & 57.04 \\ \text{Cumulative removing (%)} & 17.04 & 57.04 & 57.04 & 57.04 & 57.04 \\ \text{Cumulative removing (%)} & 17.04 & 57.04 & 57.04 & 57.04 \\ \text{Cumulative removing (%)} & 17.04 & 57.04 & 57.04 & 57.04 \\ \text{Cumulative removing (%)} & 17.04 & 57.04 & 57.04 & 57.04 & 57.04 \\ \text{Cumulative removing (%)} & 17.04 & 57.04 & 57.04 & 57.04 & 57.04 \\ \text{Cumulative removing (%)} & 17.04 & 57.04 & 57.04 & 57.04 & 57.04 \\ $	S-1.	0.07	0.07	0.56	0.28	-0.52	0.03	-0.26	-0.21	-0.20	-0.09	0.03	84.35
Total contribution (%) 17.03 12.09 9.95 8.46 7.77 6.54 5.79 4.51 3.89 3.59 3.2 Cumulative promortion (%) 17.03 29.12 39.07 47.53 55.30 61.85 67.64 72.15 76.04 79.63 82.6	Occlusal wear of UM1	0.09	-0.08	-0.07	-0.57^{***}	0.07	0.10	-0.21	0.53^{***}	-0.14	0.34^{*}	0.21	85.66
Cumulative pronortion (%) 17.03 29.12 39.07 47.53 55.30 61.85 67.64 72.15 76.04 79.63 82.5	Total contribution (%)	17.03	12.09	9.95	8.46	7.77	6.54	5.79	4.51	3.89	3.59	3.36	82.99
	Cumulative proportion (%)	17.03	29.12	39.07	47.53	55.30	61.85	67.64	72.15	76.04	79.63	82.99	82.99

exceeded 80%. ²p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction cosine for the superior-inferior axis. * P < 0.05; ** P < 0.01; *** P < 0.001, by a two-tailed bootstrap test.

Three-Dimensional Structural Deviations at Cranial Landmarks

valuation Fac I II II IV V Node 5 (ft) of Element 1: 1st p.v. 0.15 0.02 0.78^{**} 0.01 0.25 $n-1$ 0.01 0.01 0.03 0.03 0.03 0.03 $n-1$ 0.04 -0.113 0.01 0.03 0.03 0.03 $n-1$ 0.04 -0.113 0.03 0.063^{**} 0.01 0.02 $n-1$ 0.51^{*} 0.01 0.03 0.063^{**} 0.016 0.02 $n-1$ 0.60^{**} 0.066^{**} 0.063^{**} 0.016 0.017 $n-1$ -0.60^{**} 0.063^{**} 0.016 0.013^{****} 0.012^{****} 0.012^{*****} Node 3 (i) of Element 2: 1st p.v. 0.011^{**} 0.013^{******} $0.013^{************************************$	V 0.25 0.25 0.18 0.25 0.18 0.03 0.17 0.03 0.17 0.10 0.17 0.12 0.12 0.12	VI 0.21 -0.00 -0.10 -0.10 -0.14 -0.14 -0.14 -0.07 -0.06 -0.08 0.24 0.24 -0.08	VII 0.15 - 0.08 0.07 - 0.02 0.37 0.07 -	V/III			
Node 5 (ft) of Element 1: 1st p.v. 0.15 0.02 0.78** 0.01 0.25 a-p 0.013 0.01 0.03 0.90*** 0.03 m-1 0.04 0.01 0.03 0.90*** 0.03 s-i 0.010 0.32 0.04 0.03 s-i 0.019 0.05 0.03 n-1 0.05 0.019 0.015 0.017 m-1 0.060* 0.011 0.42* 0.010 s-i 0.019 0.75**** 0.016 0.17 m-1 0.060* 0.011 0.42* 0.028 Node 3 (i) of Element 2: 1st p.v. 0.01 -0.013 0.04 -0.05 0.12 m-1 0.01 -0.13 0.04 -0.05 0.017 m-1 0.01 -0.13 0.04 -0.05 0.017 m-1 0.01 -0.017 0.13 0.04 -0.05 0.017 m-1 0.01 -0.07 0.13 0.04 -0.05 0.017 m-1 0.01 -0.07 0.13 0.04 -0.05 0.017 Node 8 (SCH) of Element 2: 1st p.v. 0.11 0.01 -0.04 0.04 0.040 m-1 0.01 -0.07 0.13 0.04 -0.05 0.017 Node 8 (SCH) of Element 2: 1st p.v. 0.11 0.01 -0.04 0.04 0.040 m-1 0.01 -0.017 0.13 -0.024 0.03 m-1 0.010 -0.017 0.013 -0.024 0.03 Node 1 (g) of Element 3: 1st p.v. 0.10 0.010 0.24 0.000 0.017 m-1 0.05 0.089*** 0.010 0.010 0.015 m-1 0.02 0.020 0.000 0.015 m-1 0.02 0.000 0.015 0.000 0.015 0.010 0.024 0.000 0.015 0.015 0.000 0.015 0.010 0.024 0.000 0.015 0.015 0.000 0.010 0.015 0.000 0.015 0.000 0.015 0.000 0.010 0.015 0.000 0.015 0.000 0.015 0.010 0.024 0.000 0.015 0.000 0.015 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.015 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.010 0.024 0.000 0.015 0.000 0.000 0.000 0.010 0.024 0.000 0.015 0.000 0.000 0.000 0.010 0.024 0.000 0.015 0.000 0.000 0.000 0.000 0.000 0.000 0.015 0.0000 0.000 0.000 0	$\begin{array}{c} 1 \\ 2^{*} \\ 0.25 \\ 0.18 \\ 0.03 \\ 0.03 \\ 0.017 \\ 0.017 \\ 0.17 \\ 0.17 \\ 0.128 \\ 0.17 \\ 0.128 \\ 0.17 \\ 0.128 \\ 0.1$	0.21 - 0.00 - 0.10 - 0.10 - 0.14 - 0.07 - 0.06 - 0.30 0.24 - 0.24	0.15 - 0.08 - 0.07 - 0.37 - 0.07 - 0.05 -	111 A	IX	x	IX
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 2^{*}\\ 0.18\\ 0^{***}\\ 5\\ 6\\ 0.17\\ 2^{*}\\ 0.17\\ 0.12\\ 9\\ 0.17\\ 0.12\\ 0.17\\ 0.12\\ 0.1$	$\begin{array}{c} -0.00\\ -0.10\\ -0.10\\ -0.07\\ -0.06\\ -0.30\\ 0.24\\ 0.08\\ \end{array}$	0.08 0.07 0.37 0.05 0.05	- 0.02	-0.04	-0.05	- 0.06
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 0^{***} & 0.03 \\ 5 & 0.08 \\ 6 & 0.17 \\ 22^{*} & 0.10 \\ 9 & -0.28 \\ 0.12 \\ 0.10 \\ 0.12 \\ 0.12 \\ 0.12 \\ 0.12 \end{array}$	$\begin{array}{c} -0.10\\ -0.00\\ 0.14\\ -0.07\\ -0.30\\ 0.08\\ 0.24\\ 0.24\\ \end{array}$	0.07 - 0.02 0.37 - 0.05	0.11	-0.00	-0.72^{***}	0.33^{*}
Node 6 (STH) of Element 1: 1st p.v. $0.51^* - 0.10 0.32 - 0.19 - 0.04 - 0.08$ $a-p$ $0.30 0.03 - 0.63^* - 0.16 0.17$ $m-1 - 0.60^* 0.06 - 0.11 0.42^* 0.10$ $s-i - 0.08 - 0.19 0.73^{***} - 0.09 - 0.28$ Node 3 (i) of Element 2: 1st p.v. 0.01 - 0.13 0.04 - 0.05 0.12 m-1 - 0.07 - 0.07 0.13 - 0.24 0.35 m-1 - 0.07 - 0.07 0.13 - 0.24 0.35 m-1 - 0.07 - 0.07 0.13 - 0.24 0.35 m-1 - 0.07 - 0.07 0.13 - 0.09 - 0.07 Node 8 (SCH) of Element 2: 1st p.v. 0.11 0.01 - 0.04 - 0.06 - 0.12 Node 8 (SCH) of Element 2: 1st p.v. 0.11 0.01 - 0.04 - 0.03 - 0.03 - 0.003 - 0.03 - 0.003	5 - 0.08 6 - 0.17 2 2 * 0.17 9 - 0.28 0.12 0.12	- 0.00 - 0.14 - 0.07 - 0.30 - 0.30 0.24 - 0.24	0.02 0.37 0.07 0.05	- 0.20	0.03	0.05	0.04
Node 6 (STH) of Element 1: 1st p.v. $0.51^* - 0.13 0.16 0.15 0.29$ $a-p 0.30 0.03 -0.63^* - 0.16 0.17$ $m-1 -0.60^* 0.06 -0.11 0.42^* 0.10$ $s-i -0.08 -0.19 0.73^{***} -0.09 -0.28$ Node 3 (i) of Element 2: 1st p.v. $0.01 -0.13 0.04 -0.05 0.12$ m-1 -0.07 -0.07 0.13 -0.24 0.35 m-1 -0.07 -0.07 0.13 -0.24 0.35 m-1 -0.07 -0.07 0.08 -0.09 0.07 s-i $ -0.17 0.18 -0.15 0.15 -0.40$ Node 8 (SCH) of Element 2: 1st p.v. $0.11 0.01 -0.04 0.04 0.08^{***} -0.12 0.13 0.13 -0.10$ $m-1 -0.97^{***} -0.24 -0.15 0.13 -0.10$ Node 1 (g) of Element 3: 1st p.v. $0.10 -0.02 -0.02 -0.02 -0.02 0.012 -0.02 -0.02 -0.02 -0.02 -0.02 -0.02 -0.012 -0.02$	5 0.29 6 0.17 9 -0.28 5 0.12 0.12	0.14 - 0.07 - 0.14 - 0.06 - 0.30 0.24 0.24	0.37 0.07 - 0.05	0.06	0.18	0.78^{***}	-0.28
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccc} 6 & 0.17 \\ 2^* & 0.10 \\ 9 & -0.28 \\ 5 & 0.12 \\ 0.12 \\ \end{array}$	- 0.07 - 0.06 - 0.30 0.24 0.24	0.07 - 0.05	0.16	-0.10	0.31	-0.37
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 2^{*} \\ 9 \\ 5 \\ 0.12 \\ 0.12 \\ 0.12 \\ 0.25 \\ $	- 0.06 - 0.30 0.08 0.24	0.05	- 0.08	0.23	0.37^{**}	-0.12
	$\begin{array}{c} 9 & -0.28 \\ 5 & 0.12 \\ 0.35 \end{array}$	- 0.30 0.08 0.24		0.34^{*}	-0.26	-0.30^{*}	-0.10
Node 3 (i) of Element 2: 1st p.v. 0.01 -0.13 0.04 -0.05 0.12 m–1 -0.07 0.21 -0.07 0.13 -0.24 0.35 m–1 -0.07 0.07 0.08 -0.09 0.07 s-i -0.17 0.18 -0.15 0.15 -0.40 Node 8 (SCH) of Element 2: 1st p.v. 0.11 -0.01 0.01 -0.04 0.89 ⁴⁴¹ m–1 -0.90^{***} 0.07 0.13 -0.13 -0.10 m–1 -0.49^{***} -0.24 -0.15 0.03 -0.00 s-i 0.00^{***} 0.07 0.13 -0.02 -0.03 m–1 -0.49^{***} -0.24 -0.15 -0.02 -0.03 Node 1 (g) of Element 3: 1st p.v. -0.20 0.10 0.24 0.09 -0.17 m–1 0.05 -0.89^{***} 0.10 -0.04 0.05 -0.00 0.15 m–1 0.02 -0.02 0.000 -0.02	5 0.12 1 0.35	0.08 0.24	0.33* -	- 0.19	0.05	0.08	0.07
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1 0.25	0.24	0.13 -	- 0.03	-0.14	-0.04	0.82^{***}
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	t.0.0	0000	0.43^{*}	0.01	0.25	0.43^{**}	-0.34
Node 8 (SCH) of Element 2: 1st p.v. 0.17 0.18 -0.15 0.15 -0.40 a-p -0.90^{***} 0.01 -0.04 0.04 0.89^{***} m-l -0.90^{***} 0.07 0.13 -0.10 m-l -0.49^{***} 0.07 0.13 -0.10 s-i 0.86^{***} -0.01 -0.04 0.02 -0.03 Node 1 (g) of Element 3: 1st p.v. -0.20 0.10 0.24 0.09 -0.17 a-p 0.10 -0.02 -0.00 0.15 m-l 0.05 -0.89^{****} 0.10 -0.04 0.00 0.15 m-l 0.05 -0.89^{****} 0.10 -0.04 0.00 0.15 m-l 0.05 -0.89^{****} 0.10 -0.04 0.02 -0.017	9 0.07	- 0.09	0.82*** -	-0.14	0.05	-0.03	-0.19
Node 8 (SCH) of Element 2: 1st p.v. 0.11 0.01 -0.04 0.04 0.04 0.89^{44} $a-p$ -0.90^{***} 0.07 0.13 0.13 -0.10 $m-l$ -0.49^{***} -0.24 -0.15 -0.02 -0.03 $s-i$ 0.86^{***} -0.01 -0.04 0.20 -0.02 Node 1 (g) of Element 3: 1st p.v. -0.20 0.10 0.24 0.09 -0.17 a-p 0.10 -0.02 -0.02 -0.00 $0.15m-l 0.05 -0.89^{***} 0.10 -0.04 0.02 -0.17s-i -0.02 0.50^{***} 0.10 -0.04 0.02 0.11$	5 - 0.40	0.08 -	0.01	0.19	0.05	-0.24	0.71^{***}
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$4 0.89^{***}$	0.00	0.11 -	- 0.10	-0.00	-0.04	-0.02
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3 - 0.10	0.03 -	0.14 -	- 0.05	-0.06	-0.02	0.06
s-i 0.86^{***} -0.01 -0.04 0.20 -0.02 Node I (g) of Element 3: 1st p.v. -0.20 0.10 0.24 0.09 -0.17 $a-p$ 0.10 -0.22 -0.02 0.10 0.24 0.09 -0.17 $m-l$ 0.10 -0.22 -0.02 -0.02 -0.017 -0.17 $m-l$ 0.10 -0.02 -0.02 -0.00 0.15 $m-l$ 0.05 -0.89^{***} 0.10 -0.04 0.02 $s-i$ -0.02 0.50^* 0.37 -0.28 0.11	2 - 0.03	0.29 -	0.43 -	- 0.11	0.02	0.27	0.21
Node I (g) of Element 3: 1st p.v. -0.20 0.10 0.24 0.09 -0.17 a-p 0.10 -0.02 -0.060 -0.00 0.15 m-l 0.05 -0.89^{***} 0.10 -0.04 0.02 s-i -0.02 0.50 [*] 0.37 -0.28 0.11	0 - 0.02	- 0.05 -	0.02	0.11	-0.05	0.10	0.03
$a-p$ 0.10 -0.02 -0.60 -0.00 0.15 $m-l$ 0.05 -0.89^{***} 0.10 -0.04 0.02 $s-i$ -0.02 0.50^* 0.37 -0.28 0.11	9 - 0.17	0.03 -	0.03 -	- 0.03	0.13	-0.70^{***}	-0.29
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0 0.15	-0.06	- 90.0	- 0.14	-0.30	0.26	0.44^{**}
s_{-1} -0.02 0.50^{*} 0.37 -0.28 0.11	4 0.02	0.13 -	0.13	0.09	-0.06	-0.07	-0.03
	8 0.11	- 0.20 -	0.22	0.02	0.35^{*}	0.07	-0.34^{*}
Node 7 (zm) of Element 3: 1st p.v0.07 -0.18 0.08 -0.11 -0.03	1 - 0.03	0.92^{***}	- 0.07	- 0.08	-0.12	-0.01	0.12
a-p -0.01 0.13 -0.00 0.04 0.09	4 0.09	-0.08	0.01	0.10	0.93^{***}	-0.01	-0.09
m-l -0.31 0.09 0.04 0.07 0.34	7 0.34	0.14	0.13	0.10	-0.50^{**}	-0.22	0.41^{**}
s-i 0.41** 0.00 0.09 0.06 - 0.55**	$6 - 0.55^{**}$	0.19 -	0.25 -	- 0.31	-0.35^{*}	-0.13	-0.18
Occlusal wear of UM1 $0.15 - 0.09 - 0.00 - 0.23 - 0.06$	3 -0.06	-0.08	0.15	0.85^{***}	0.10	0.00	0.04

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Moriabla ²					Factor l	oadings					Total
Variable	PC I	П	II	IV	>	ΙΛ	ΠΛ	VIII	IX	x	variance (%)
Node 5 (ft) of Element 1: 1st p.v.	-0.32	0.15	0.56***	-0.36^{***}	0.42***	0.14*	0.08	-0.18^{**}	0.09	0.06	81.59
a-p	0.56^{***}	-0.05	0.53	-0.05	-0.08	-0.34	0.11	0.27	0.30^{*}	-0.03	90.26
m_l	0.67^{***}	-0.02	-0.45	-0.14	-0.03	0.23	-0.23	-0.12	0.18	0.12	83.69
S-i	-0.61^{***}	-0.06	-0.07	0.29	-0.18	-0.08	0.09	-0.00	-0.29	0.38^{*}	73.71
Node 6 (STH) of Element 1: 1st p.v.	-0.18	0.62^{***}	0.21^{*}	-0.14	0.48^{***}	0.16^{*}	0.39^{***}	-0.01	-0.15	-0.07	91.31
a-p	0.43^{**}	0.15	-0.08	-0.07	-0.00	-0.23	0.52^{*}	0.48^{*}	-0.07	-0.11	78.61
m_l	0.73^{***}	-0.11	-0.26	-0.14	0.10	0.12	-0.29	-0.18	-0.05	0.20	81.78
Si	-0.61^{***}	-0.15	0.26	0.34	-0.26	0.01	-0.14	-0.00	0.22	0.29	79.47
Node 3 (i) of Element 2: 1st p.v.	0.24	-0.30^{***}	0.27^{***}	0.59^{***}	0.26^{***}	0.18^{***}	-0.11^{**}	0.16^{***}	-0.02	-0.18^{***}	73.71
a-p	0.02	0.27	-0.11	-0.09	-0.47	0.35	0.58^{**}	0.05	0.12	0.11	80.39
m_l	-0.51^{***}	-0.04	-0.07	-0.04	0.31	-0.26	-0.34	0.46^{*}	-0.12	-0.04	78.49
S-1	0.29	-0.49	0.42	0.48	-0.30	-0.07	-0.09	-0.20	0.05	-0.04	86.15
Node 8 (SCH) of Element 2: 1st p.v.	0.15	0.54^{***}	0.39^{*}	0.29	0.05	0.25	-0.33^{**}	0.31^{**}	0.00	-0.10	83.57
a-p	-0.29^{*}	-0.26	0.02	-0.09	-0.06	0.80^{***}	0.04	0.13	0.26	-0.04	89.25
m_l	-0.29	-0.45	-0.51	-0.19	-0.12	-0.44	0.11	0.01	-0.01	-0.05	80.61
S-i	0.38^{**}	0.32	0.46	-0.03	0.05	-0.39^{*}	0.07	-0.20	-0.24	0.44^{**}	91.66
Node 1 (g) of Element 3: 1st p.v.	-0.06	-0.31^{***}	0.43^{***}	-0.50^{***}	0.00	-0.02	-0.25^{**}	0.15	-0.21^{**}	-0.05	67.07
a-p	0.07	-0.03	-0.15	0.68^{*}	0.23	-0.09	0.41	-0.31	-0.03	-0.19	85.42
m-l	0.00	0.40	-0.28	-0.12	0.40	-0.09	-0.10	0.04	0.52^{**}	0.34^{*}	82.32
S-I.	0.17	-0.13	0.34	-0.42	-0.57	0.21	0.08	0.13	-0.26^{*}	0.08	80.49
Node 7 (zm) of Element 3: 1st p.v.	0.04	0.61^{***}	0.10	0.50^{***}	-0.27^{***}	-0.01	-0.13^{*}	0.10^{*}	0.05	0.15^{***}	76.49
a-p	-0.01	-0.61^{**}	0.40	-0.18	0.22	-0.18	0.21	-0.15	0.38^{*}	0.01	84.80
m-l	0.31	-0.33	-0.18	0.11	0.39	0.32	0.02	0.15	-0.51^{**}	0.19	82.27
Si	-0.06	0.64^{**}	-0.13	-0.16	-0.38	-0.22	-0.29	-0.10	0.02	-0.34^{*}	85.68
Occlusal wear of UM1	0.10	-0.23	-0.18	0.17	-0.01	-0.07	0.10	0.71^{***}	0.18	0.19	70.47
Total contribution (%)	12.99	12.44	10.16	9.51	7.91	7.29	6.42	6.06	5.11	3.70	81.57
Cumulative proportion (%)	12.99	25.42	35.59	45.10	53.01	60.29	66.71	72.77	77.87	81.57	81.57
¹ The sample size is 33. The num	ber of princip	al componer	its shown he	ere was deter	rmined so tl	nat the cumu	ilative propo	ortion of the	variances o	f the princip	al components

exceeded 80%.

² p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction cosine for the superior-inferior axis.

Useriable ²					Factor I	oadings				
VallaUIC	Fac I	Π	III	IV	Λ	Ν	IIA	ΠIΛ	IX	Х
Node 5 (ft) of Element 1: 1 st p.v.	- 0.15	-0.01	0.12	- 0.25	0.67*	-0.01	- 0.05	-0.31	0.38	0.13
a-p	0.23	0.17	0.28	-0.16	-0.12	-0.35	0.05	0.46	0.60^{**}	-0.06
m_l	0.72^{***}	-0.14	0.01	-0.01	-0.39^{*}	0.04	0.20	-0.05	-0.13	0.30^{*}
s-i	-0.76^{*}	-0.17	-0.17	0.06	-0.06	-0.07	0.03	-0.11	-0.28	-0.02
Node 6 (STH) of Element 1: 1st p.v.	-0.03	-0.00	0.22	0.12	0.90^{***}	-0.09	0.08	0.03	-0.13	0.10
a-p	0.24	-0.00	-0.04	0.07	0.16	-0.20	0.17	0.78^{***}	-0.03	-0.09
m-l	0.71^{***}	-0.31	0.02	-0.08	-0.34^{*}	-0.20	0.06	-0.14	-0.06	0.17
s-i	-0.78^{**}	0.07	0.12	-0.03	-0.25	0.15	-0.00	-0.22	0.16	0.10
Node 3 (i) of Element 2: 1st p.v.	0.03	-0.36	0.45	0.33	-0.19	0.14	-0.26	0.08	0.29	-0.28
a–p	-0.09	0.12	-0.01	-0.01	0.12	0.17	0.81^{***}	0.22	-0.17	0.01
m_l	-0.35	0.00	-0.09	-0.18	0.11	0.13	-0.71^{***}	0.17	-0.18	0.14
S-i	-0.08	-0.10	0.22	0.15	-0.55^{*}	-0.14	0.07	-0.13	0.49^{**}	-0.44^{*}
Node 8 (SCH) of Element 2: 1st p.v.	0.03	0.10	0.88^{***}	-0.06	0.10	-0.00	-0.13	0.08	-0.14	0.00
a-p	-0.12	-0.22	0.12	-0.20	0.06	0.82^{***}	0.27	-0.15	0.12	0.04
m_l	-0.14	0.10	-0.81^{***}	0.03	-0.23	0.07	-0.19	0.15	-0.06	0.00
S-i	0.03	-0.07	0.23	-0.11	0.13	-0.89^{***}	0.13	-0.04	0.13	0.04
Node 1 (g) of Element 3: 1st p.v.	0.02	-0.07	-0.06	-0.67^{*}	0.10	-0.02	-0.26	-0.06	0.24	-0.26
a-p	-0.05	-0.14	-0.01	0.89^{***}	0.02	-0.08	0.06	0.00	0.07	-0.19
m_l	0.13	0.10	0.05	0.11	0.15	-0.03	-0.08	0.04	-0.01	0.87^{***}
S-i	0.02	-0.01	0.02	-0.67^{**}	-0.08	-0.06	0.44^{*}	0.07	0.02	-0.39^{*}
Node 7 (zm) of Element 3: 1st p.v.	-0.24	0.24	0.62^{*}	0.21	-0.15	-0.22	0.15	0.07	-0.32	0.13
a-p	-0.04	-0.09	-0.28	-0.06	0.03	0.03	-0.06	-0.04	0.86^{***}	-0.01
m_l	0.24	-0.84^{**}	-0.01	0.03	-0.00	0.02	-0.11	0.07	-0.17	-0.14
s-i	0.13	0.76^{***}	0.13	-0.09	0.02	-0.12	-0.03	-0.10	-0.46^{**}	-0.01
Occlusal wear of UM1	-0.13	-0.23	0.02	-0.04	-0.29	0.17	-0.09	0.68^{**}	0.04	0.21

Table 5. Rotated solution of the first ten principal components extracted from the correlations between the linearized first principal values and their direction cosines at

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Table 6. Principal component anal STH, i, SCH, g, and zm in the th	ysis of the co nree right eler	rrelations be nents, and th	stween the l ne degree of	inearized fir occlusal we	st principal ar on the ma	values and t axillary first	heir directic molar in Ind	n cosines at ians. ¹	six craniofa	cial landma	rks, i.e., ft,
Voriabla ²					Factor	loadings					Total
Vallaulo	PC I	Π	III	IV	Λ	Ν	ΝП	VIII	IX	Х	variance (%)
Node 5 (ft) of Element 1: 1 st p.v.	0.52	-0.45	-0.10	-0.29	-0.45	0.10	-0.08	0.10	-0.06	0.16	83.08
a-p	-0.35	-0.12	0.71	0.08	0.26	0.12	-0.07	0.10	-0.30	0.06	83.60
m-l	0.38	0.49	-0.18	0.15	-0.20	-0.46	0.05	-0.26	0.26	-0.08	82.43
S—i	0.18	-0.33	-0.60	0.11	-0.09	0.01	-0.08	-0.27	-0.06	-0.46^{*}	81.82
Node 6 (STH) of Element 1: 1st p.v.	0.34	-0.13	-0.68	-0.27	-0.03	0.17	-0.21	0.15	-0.08	0.23	82.16
a-p	-0.57	0.22	0.04	-0.33	0.55	-0.07	-0.10	-0.15	0.13	-0.18	86.67
m-l	0.42	0.11	0.41	0.17	-0.20	-0.20	0.54^{*}	-0.18	-0.23	0.01	84.28
S-i	0.46	-0.40	-0.03	0.25	-0.35	0.03	-0.36	0.14	0.23	-0.01	76.40
Node 3 (i) of Element 2: 1st p.v.	0.17	-0.62	0.09	-0.08	0.13	0.22	0.38	-0.21	0.13	-0.08	71.03
a-p	-0.77	-0.02	0.02	-0.10	-0.31	-0.25	-0.10	0.05	0.23	-0.03	82.53
m_l	0.45	0.36	0.51	0.16	-0.19	0.07	-0.38	0.07	-0.26	0.04	87.42
S-i	0.38	-0.48	0.02	-0.01	0.33	0.41	0.33	-0.23	0.03	0.20	85.66
Node 8 (SCH) of Element 2: 1st p.v.	0.26	-0.15	0.25	-0.51	0.06	0.02	-0.14	0.43	0.36	-0.29	83.74
a-p	-0.30	-0.41	0.43	-0.44	-0.36	-0.11	-0.00	-0.32	0.08	-0.01	89.01
m-l	-0.41	0.09	-0.30	-0.37	0.04	0.47	-0.18	-0.34	0.08	0.30	86.62
S-i	0.04	0.44	-0.60	0.28	0.39	-0.05	0.17	0.20	-0.12	0.08	87.27
Node 1 (g) of Element 3: 1st p.v.	0.01	-0.45	0.04	0.33	0.50	-0.22	-0.34	0.08	-0.07	0.15	76.05
ap	0.16	0.67	-0.14	-0.54	-0.14	-0.01	-0.07	-0.15	-0.10	0.23	89.37
m-l	-0.39	0.09	-0.12	0.27	-0.26	0.48	0.35	0.40	0.09	-0.18	86.82
S-i	-0.09	-0.50	-0.18	0.44	0.23	-0.33	-0.25	-0.24	0.12	0.09	79.36
Node 7 (zm) of Element 3: 1st p.v.	0.15	-0.19	0.16	-0.24	0.19	-0.53	0.29	0.28	0.28	0.43	89.18
ap	-0.27	0.13	0.22	0.57	-0.17	0.42	-0.08	0.02	0.39	0.29	90.73
m_l	0.48	0.10	0.40	-0.19	0.43	0.23	-0.29	-0.05	-0.07	-0.19	79.30
S-i	-0.30	-0.47	-0.31	-0.31	0.09	-0.14	0.14	0.31	-0.32	-0.04	74.77
Occlusal wear of UM1	-0.54	-0.35	-0.03	0.10	-0.44	-0.14	-0.11	-0.02	-0.42^{*}	0.09	84.06
Total contribution (%)	14.38	12.99	11.61	9.17	8.68	7.02	6.00	4.91	4.56	4.00	83.34
Cumulative proportion (%)	14.38	27.38	38.99	48.15	56.84	63.86	69.86	74.77	79.33	83.34	83.34
¹ The sample size is 35. The numb	er of principa	l componen	ts shown he	re was deter	mined so th	lat the cumu	lative propo	tion of the	variances of	the principa	l components

² p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction cosine for the superior-inferior exceeded 80%. axis.

* P < 0.05; ** P < 0.01; *** P < 0.001, by a two-tailed bootstrap test.

six craniofacial landmarks, i.e.,	ft, STH, i, S	CH, g, and zm	in the three ri	ght elements,	and the degre	e of occlusal	wear on the m	axillary first 1	nolar in India	ns. ¹
Voriabla ²					Factor	loadings				
VallaUlC	Fac I	Π	III	IV	>	ΙΛ	ΠΛ	VIII	IX	X
Node 5 (ft) of Element 1: 1st p.v.	0.81^{*}	0.04	-0.07	- 0.22	-0.10	-0.24	0.20	0.00	0.10	0.05
a-p	-0.36	0.30	0.19	-0.29	0.11	0.17	-0.04	0.66^{***}	-0.08	0.14
m_l	0.03	0.08	0.23	0.14	-0.09	-0.00	-0.22	-0.82^{***}	-0.08	0.03
S—i	0.24	-0.23	-0.06	0.10	0.25	-0.33	0.19	-0.27	0.01	-0.64^{**}
Node 6 (STH) of Element 1: 1 st p.v.	0.53	-0.05	-0.52	0.38	-0.02	-0.34	0.07	-0.07	0.05	-0.03
a-p	-0.82^{*}	-0.02	-0.34	-0.07	0.06	-0.13	-0.10	0.06	0.19	0.02
m_l	0.08	0.20	0.70^{***}	-0.09	-0.27	-0.02	0.25	-0.18	-0.31	0.17
S-i	0.72	0.09	0.07	-0.11	0.33	0.18	0.00	-0.12	0.23	-0.13
Node 3 (i) of Element 2: 1st p.v.	0.09	-0.13	0.10	-0.24	0.12	-0.07	0.77^{***}	0.08	0.11	-0.04
a-p	-0.26	-0.56	-0.15	-0.43	0.04	0.13	-0.47^{*}	0.06	0.02	0.04
m_l	0.27	0.75**	0.27	-0.03	-0.15	0.20	-0.32	0.04	-0.05	-0.01
S—i	0.15	0.15	-0.07	0.06	0.10	0.01	0.88^{***}	0.11	-0.04	0.06
Node 8 (SCH) of Element 2: 1st p.v.	0.12	0.14	0.01	-0.18	-0.12	-0.15	0.03	0.07	0.84^{***}	0.16
a-p	-0.02	-0.13	-0.05	-0.92^{***}	-0.06	-0.10	0.07	0.09	-0.00	0.08
m_l	-0.17	-0.08	-0.85^{***}	-0.11	-0.20	0.09	0.09	0.06	-0.19	-0.09
Si	-0.18	-0.13	-0.07	0.87^{***}	-0.00	-0.08	-0.09	-0.14	-0.16	0.00
Node 1 (g) of Element 3: 1st p.v.	-0.01	0.15	0.00	0.12	0.80^{***}	-0.06	0.05	0.24	-0.00	0.13
a-p	-0.04	0.29	-0.37	0.08	-0.62^{**}	-0.22	-0.27	-0.33	-0.13	0.19
m-l	-0.02	-0.52^{*}	0.10	0.22	-0.35	0.45	-0.01	0.35	0.09	-0.28
s—i	0.02	-0.15	-0.03	-0.04	0.85^{***}	0.00	0.08	-0.12	-0.17	-0.04
Node 7 (zm) of Element 3: 1st p.v.	0.04	-0.15	0.15	-0.03	0.14	-0.18	0.12	-0.10	0.19	0.86^{***}
a-p	0.01	-0.07	-0.08	0.00	0.07	0.93^{***}	-0.04	0.09	-0.12	-0.01
m_l	-0.10	0.79^{***}	0.02	0.02	0.00	-0.08	0.19	0.07	0.34	-0.06
S-i	0.04	-0.46^{*}	-0.10	0.01	0.10	-0.56^{**}	0.04	0.45^{*}	0.05	0.06
Occlusal wear of UM1	0.15	-0.39	-0.01	-0.38	0.15	-0.10	-0.32	0.40	-0.45^{*}	-0.15
¹ The sample size is 35. The cumu	lative propor	tion of the vari	ances of the to	en principal co	omponents is	83.34%.				
² p.v.: principal value; a–p: directio.	n cosine for t	he anterior-pos	terior axis; m-	-l: direction co	sine for the m	edial-lateral a	xis; s-i: directi	ion cosine for	the superior-in	nferior axis.
*P < 0.05; **P < 0.01; ***P < 0.01	001, by a two	-tailed bootstr	ap test.							

Table 7. Rotated solution of the first ten principal components extracted from the correlations between the linearized first principal values and their direction cosines at

Weishlo2					Factor	loadings					Total
Valiaure	PC I	Π	III	IV	>	ΙΛ	ΠΛ	VIII	IX	Х	variance (%)
Node 5 (ft) of Element 1: 1st p.v.	-0.21	- 0.76	-0.26	-0.07	0.33	0.21	0.09	0.04	-0.18	0.09	90.05
a-p	0.36	0.27	-0.28	0.66	-0.11	0.24	-0.03	0.21	0.07	0.31^{*}	93.97
m_l	0.48	-0.16	0.56	-0.23	-0.02	-0.21	-0.22	0.25	-0.20	-0.03	81.25
S—I.	-0.50	0.34	0.29	0.11	-0.03	0.07	0.21	-0.35	0.28	-0.44^{*}	91.60
Node 6 (STH) of Element 1: 1st p.v.	-0.37	-0.31	-0.51	-0.21	0.36	0.03	0.06	-0.02	-0.48^{*}	-0.03	90.79
a-p	0.27	0.73	-0.41	0.21	-0.10	-0.00	0.08	-0.11	0.10	0.03	85.66
m-l	0.42	-0.16	0.50	0.11	-0.04	-0.35	-0.31	-0.06	-0.27	-0.23	81.06
S-i	-0.50	-0.27	0.29	0.33	0.29	0.08	0.18	-0.05	0.29	0.19	74.98
Node 3 (i) of Element 2: 1st p.v.	0.38	-0.35	-0.15	0.11	0.57^{*}	0.15	0.10	-0.02	0.14	-0.32	77.81
ap	-0.35	0.07	0.46	0.36	-0.02	0.05	0.55^{*}	0.15	-0.27	-0.10	88.13
m-l	-0.53	-0.18	-0.08	-0.32	-0.18	-0.30	-0.19	0.06	0.19	-0.03	61.15
S-i.	0.65	-0.01	-0.36	-0.08	0.29	0.18	-0.40	0.07	0.23	-0.13	91.68
Node 8 (SCH) of Element 2: 1st p.v.	-0.32	-0.45	-0.21	0.41	0.12	-0.37	-0.13	-0.24	0.07	0.12	75.16
a-p	0.14	-0.63	0.29	0.08	-0.52	0.38	0.01	-0.14	0.05	-0.08	94.29
m-l	-0.24	-0.14	0.46	0.25	0.43	-0.21	-0.27	-0.09	0.13	0.42^{*}	85.59
Si	-0.22	0.73	-0.20	-0.18	0.41	-0.18	0.08	0.25	-0.11	-0.01	93.55
Node 1 (g) of Element 3: 1st p.v.	0.57	-0.15	-0.16	0.28	0.05	-0.19	0.44	-0.27	-0.24	0.09	82.50
a-p	-0.49	0.01	-0.31	-0.18	-0.43	0.43	-0.11	0.03	-0.12	0.15	79.34
m-l	-0.42	0.20	0.06	0.49	0.18	-0.12	-0.13	0.58^{**}	-0.01	-0.26	93.08
S-1	0.56	0.16	0.17	-0.32	0.30	-0.00	0.38	-0.28	0.12	0.08	79.85
Node 7 (zm) of Element 3: 1st p.v.	0.10	-0.18	-0.25	0.71	-0.01	0.18	-0.29	-0.19	-0.10	-0.27	83.83
a-p	0.08	-0.43	0.07	-0.24	0.20	0.35	0.20	0.44	0.34	-0.08	77.19
m-l	0.18	-0.33	-0.25	0.03	-0.26	-0.59^{*}	0.21	0.16	0.30	0.08	78.04
S-i	-0.22	0.39	0.39	-0.13	0.35	0.34	-0.34	-0.38	-0.04	0.10	87.21
Occlusal wear of UM1	0.37	0.11	0.45	0.14	-0.00	0.34	0.07	0.32	-0.10	0.21	64.67
Total contribution (%)	15.13	13.57	10.78	9.10	7.87	7.00	5.99	5.67	4.33	3.85	83.30
Cumulative proportion (%)	15.13	28.70	39.49	48.59	56.45	63.46	69.45	75.12	79.45	83.30	83.30

² p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction cosine for the superior-inferior

axis. * P<0.05; ** P<0.01; *** P<0.001, by a two-tailed bootstrap test.

six craniofacial landmarks, i.e.,	ft, STH, i, SO	H, g, and zm	in the three le	eft elements, a	ind the degree	e of occlusal w	ear on the ma	xillary first m	olar in Indians	.'
Vicition 2					Factor	loadings				
VallaDIC	Fac I	Π	III	IV	>	ΙΛ	IIA	VIII	IX	X
Node 5 (ft) of Element 1: 1st p.v.	0.02	-0.28	-0.14	-0.09	0.18	-0.08	0.22	0.02	-0.82^{***}	0.20
a-p	0.16	0.02	-0.22	0.86^{***}	0.03	-0.13	-0.12	0.21	0.21	0.01
m_l	0.07	-0.09	0.86^{***}	0.02	-0.04	-0.02	0.20	-0.11	0.08	-0.03
S-i	-0.50	0.01	-0.34	-0.42	0.18	0.34	-0.12	0.09	0.45	0.03
Node 6 (STH) of Element 1: 1st p.v.	-0.00	0.19	-0.21	-0.21	0.04	0.03	-0.09	0.06	-0.87^{***}	-0.08
a-p	0.17	0.41	-0.35	0.38	0.03	-0.02	-0.34	-0.08	0.42	-0.31
m_l	0.01	-0.18	0.82^{***}	-0.02	0.17	-0.00	-0.24	0.03	0.14	0.03
S-1.	-0.37	-0.13	-0.26	-0.07	0.11	0.07	0.18	0.12	-0.05	0.68^{***}
Node 3 (i) of Element 2: 1st p.v.	0.18	-0.06	0.03	0.09	0.79^{***}	-0.03	0.20	-0.09	-0.23	0.04
a-p	-0.91^{***}	0.01	0.04	0.14	0.01	0.05	0.06	0.12	0.01	0.07
m_l	0.07	0.01	-0.11	-0.62^{***}	-0.32	-0.18	0.05	0.22	-0.06	0.13
S—i	0.78***	0.05	0.08	0.23	0.44^{*}	0.03	0.13	-0.02	0.03	-0.18
Node 8 (SCH) of Element 2: 1st p.v.	0.02	-0.16	-0.16	-0.16	0.12	-0.31	-0.39	0.21	-0.27	0.54^{*}
a-p	-0.09	-0.95^{***}	0.09	0.02	-0.04	-0.03	0.14	-0.02	0.00	-0.07
m-l	-0.03	0.06	0.22	0.00	-0.03	0.17	-0.03	0.04	0.01	0.88^{***}
S-1.	-0.06	0.93^{***}	-0.13	-0.03	-0.06	0.17	0.01	0.06	0.03	-0.12
Node 1 (g) of Element 3: 1st p.v.	-0.12	-0.09	0.11	0.41	0.35	-0.38	-0.34	-0.47	-0.14	-0.09
a-p	0.04	-0.21	-0.48^{*}	-0.08	-0.56^{**}	0.20	0.04	0.23	-0.21	-0.25
m-l	-0.29	0.36	0.03	0.08	0.10	-0.03	0.09	0.81^{***}	0.07	0.15
S—I.	0.04	0.16	0.13	0.09	0.30	0.06	0.14	-0.78^{***}	0.16	-0.06
Node 7 (zm) of Element 3: 1st p.v.	0.12	-0.35	-0.12	0.32	0.42	0.05	-0.45^{*}	0.45*	-0.07	0.02
a-p	0.05	-0.19	-0.04	-0.03	0.23	-0.09	0.81^{***}	-0.00	-0.15	0.01
m-l	0.10	-0.05	0.03	-0.12	-0.00	-0.86^{***}	-0.01	-0.06	0.08	0.07
Si	0.04	0.14	0.00	-0.08	-0.06	0.86^{***}	-0.07	-0.12	0.13	0.26
Occlusal wear of UM1	-0.14	-0.09	0.33	0.56^{**}	-0.06	0.20	0.35	-0.06	0.17	0.00
¹ The sample size is 35. The cumul	lative proport	ion of the vari	ances of the t	en principal co	omponents is	83.30%.				
² p.v.: principal value; a-p: directio	n cosine for th	ne anterior-pos	terior axis; m-	-l: direction cc	osine for the r	nedial-lateral a	xis; s-i: direct	on cosine for	the superior-ir	nferior axis.
*P < 0.05; **P < 0.01; ***P < 0.01	001, by a two	-tailed bootstr	ap test.							

Table 9. Rotated solution of the first ten principal components extracted from the correlations between the linearized first principal values and their direction cosines at

omponent analysis of the correlations between the linearized first principal values and their direction cosines at six craniofacial landmarks, i.e., ft,	d zm in the three right elements, and age in African-Americans. ¹
 Principal component analysis 	H, i, SCH, g, and zm in the three ri
Table 1	ST

	0	0		H	actor loading	S				Total
Variable	PC I	Π	III	IV	^	Ν	ΠΛ	VIII	IX	variance (%)
Node 5 (ft) of Element 1: 1st p.v.	-0.34	0.44**	-0.12	0.39***	-0.54^{***}	0.02	0.26**	-0.24^{**}	0.04	89.91
a-p	0.72^{***}	-0.05	0.27	0.09	-0.32	-0.27	0.01	-0.12	0.04	79.47
m_l	-0.32	0.32	-0.34	0.16	0.37	-0.09	-0.53^{*}	-0.01	0.23	82.10
S-i	-0.67^{***}	-0.51	0.10	-0.25	0.01	0.10	0.01	0.14	-0.00	81.15
Node 6 (STH) of Element 1: 1st p.v.	-0.53^{*}	0.41^{***}	-0.23^{**}	0.26^{***}	-0.46^{***}	-0.11	0.25^{**}	-0.11	0.06	86.92
a-p	0.38^{*}	-0.49	0.36	-0.13	-0.24	-0.20	-0.38^{*}	-0.29	0.15	88.23
m_l	0.08	0.19	-0.62	-0.42	0.20	0.12	0.22	-0.25	0.33^{*}	87.18
S-I	-0.52^{**}	0.22	0.25	0.41	-0.09	0.28	0.03	0.30^{*}	-0.21	77.49
Node 3 (i) of Element 2: 1st p.v.	0.36	0.23^{*}	0.31^{***}	-0.04	-0.06	0.47^{***}	-0.07	-0.05	0.64^{***}	92.21
a-p	0.28	-0.06	-0.48	0.13	-0.34	-0.47	-0.05	-0.25	-0.04	73.83
m_l	0.01	-0.00	0.41	-0.69^{*}	-0.08	-0.20	0.04	0.21	-0.06	73.24
S—i	-0.30	-0.06	0.45	0.31	0.15	0.62^{**}	0.00	-0.23	0.05	85.60
Node 8 (SCH) of Element 2: 1st p.v.	-0.11	0.69^{***}	0.11	-0.44^{**}	-0.29^{*}	0.10	-0.17	0.08	0.00	82.43
a-p	0.75^{***}	0.12	-0.20	-0.03	0.01	0.31	0.06	0.08	-0.19	75.80
m_l	0.00	-0.48^{*}	-0.55	0.21	0.30	0.15	0.03	-0.06	0.13	71.21
S-i	-0.74^{***}	0.05	0.20	0.10	0.07	-0.32	0.03	-0.18	0.12	75.67
Node 1 (g) of Element 3: 1st p.v.	-0.42	-0.57^{***}	-0.22	-0.18	-0.31^{**}	0.23^{**}	0.21^{**}	-0.12	0.11	80.30
a-p	0.60^{**}	0.42	0.36	0.33	-0.02	0.08	0.24	0.11	0.10	86.32
m_l	-0.30	0.41	0.08	-0.01	0.66^{**}	-0.39	0.08	-0.09	-0.01	86.50
S:	-0.19	-0.52	-0.31	-0.25	-0.34	0.34	-0.23	0.01	-0.15	76.78
Node 7 (zm) of Element 3: 1st p.v.	-0.14	-0.36^{***}	0.18^{*}	-0.30^{***}	0.03	-0.27^{***}	0.59^{***}	0.28^{**}	0.34^{***}	88.68
a-p	0.07	0.52	-0.51	-0.40	0.04	0.24	0.07	-0.06	-0.13	77.43
m_l	-0.43^{**}	0.11	0.54	-0.26	-0.06	-0.00	-0.17	-0.47^{*}	-0.04	81.15
Si	-0.08	-0.29	-0.17	0.55^{*}	-0.19	-0.19	-0.27	0.39^{*}	0.29	80.23
Age	-0.30	0.49^{*}	-0.17	-0.33	-0.36	-0.05	-0.32	0.36	0.20	87.78
Total contribution (%)	17.15	14.02	11.37	9.78	7.95	7.34	5.49	4.73	4.08	81.90
Cumulative proportion (%)	17.15	31.17	42.53	52.31	60.26	67.60	73.10	77.83	81.90	81.90
¹ The sample size is 27. The numl exceeded 80%. ² p.v.: principal value; a–p: directi	ber of principa	l components the anterior-p	shown here osterior axis.	was determin ; m-l: directio	ned so that the on cosine for	e cumulative I the medial-la	proportion of teral axis; s-	the variance: i: direction o	s of the princi osine for the	pal components superior-inferior

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axis. * $P\!<\!0.05;$ ** $P\!<\!0.01;$ *** $P\!<\!0.001,$ by a two-tailed bootstrap test.

Therefore				Fac	tor loadings				
VallaDIC	Fac I	Π	III	IV	Λ	Ν	IIV	NIII	IX
Node 5 (ft) of Element 1: 1 st p.v.	0.04	0.10	0.01	0.93^{***}	0.08	0.06	-0.09	0.05	0.04
a-p	0.33	-0.02	0.02	0.01	-0.40	-0.70^{***}	0.12	0.16	-0.04
m-l	0.15	0.14	-0.38	-0.08	0.42	0.24	-0.55^{*}	-0.29	-0.01
S—i	-0.64	-0.01	0.00	-0.16	0.46^{*}	0.24	0.27	0.18	0.02
Node 6 (STH) of Element 1: 1st p.v.	-0.03	0.19	-0.07	0.85^{***}	0.24	0.19	-0.01	-0.03	-0.11
a-p	-0.16	-0.07	0.01	-0.31	0.03	-0.84^{***}	-0.01	0.18	0.10
m_l	-0.06	0.03	0.08	0.04	-0.08	0.11	0.03	-0.92^{***}	0.02
S-i	-0.02	0.09	-0.06	0.31	0.14	0.54^{*}	-0.09	0.56^{**}	0.18
Node 3 (i) of Element 2: 1st p.v.	0.19	0.19	-0.07	-0.04	-0.23	-0.22	0.03	-0.18	0.84^{***}
a-p	0.01	-0.10	-0.20	0.31	-0.15	-0.47^{*}	-0.13	-0.25	-0.52^{***}
m_l	-0.03	0.50^{*}	0.34	-0.36	0.09	-0.13	0.44^{*}	0.09	-0.09
Si	-0.12	-0.29	0.22	0.08	0.18	0.24	-0.18	0.33	0.69^{***}
Node 8 (SCH) of Element 2: 1st p.v.	0.11	0.82^{**}	0.27	0.15	-0.01	0.09	-0.11	-0.10	0.11
a-p	0.17	-0.05	0.10	-0.15	-0.80^{***}	-0.05	-0.14	-0.16	0.02
m_l	-0.32	-0.57^{*}	-0.35	-0.12	-0.06	0.14	-0.10	-0.34	-0.05
S-i.	0.00	0.01	0.01	0.25	0.81^{***}	0.13	0.08	0.12	-0.04
Node 1 (g) of Element 3: 1st p.v.	-0.79^{***}	-0.19	-0.00	0.19	0.13	-0.00	0.28	-0.10	0.05
a-p	0.69^{***}	-0.01	0.02	0.13	-0.48^{*}	-0.10	0.09	0.18	0.31^{*}
m-l	0.56^{*}	-0.03	0.14	-0.14	0.57^{**}	0.35	-0.04	-0.18	-0.17
S—i	-0.85^{***}	0.03	-0.03	-0.07	-0.13	-0.04	-0.10	-0.00	-0.06
Node 7 (zm) of Element 3: 1st p.v.	-0.07	-0.06	-0.07	-0.09	0.18	0.01	0.91^{***}	-0.08	-0.01
a-p	-0.00	0.34	0.27	0.11	-0.29	0.32	-0.21	-0.57^{***}	-0.13
m-l	-0.08	0.20	0.53^{*}	0.04	0.59^{*}	-0.18	-0.10	0.18	0.24
S-i	-0.09	-0.10	-0.83^{***}	0.10	0.05	-0.08	-0.03	0.26	-0.05
Age	-0.10	0.86^{***}	-0.23	0.15	0.10	0.14	-0.08	-0.13	-0.03
¹ The sample size is 27. The cumuli	ative proportion	of the variances	of the nine prin	icipal componen	ts is 81.90%.				
² p.v.: principal value; a–p: directior	n cosine for the a	nterior-posterior	axis; m-l: direct	tion cosine for th	ie medial-lateral	axis; s-i: diree	ction cosine for	the superior-in	nferior axis.
* n / 0 05. ** n / 0 01. *** n / 0 0	101 by a two toil	ad hootstaan too				t.		¢	
. P<0.05; ``P<0.01; ``P<0.0	01, by a two-tail	ed bootstrap tes							

Table 11. Rotated solution of the first nine principal components extracted from the correlations between the linearized first principal values and their direction cosines

Monichlo2				Ŧ	actor loading	S				Total
VallaUIC	PC I	Π	III	IV	Λ	IV	ΠΛ	NIII	IX	variance (%)
Node 5 (ft) of Element 1: 1st p.v.	-0.54^{*}	0.44^{**}	- 0.24	0.30^{*}	-0.15	0.46^{***}	0.16	-0.18^{**}	0.02	91.85
a-p	0.60^{***}	-0.44	-0.15	0.22	0.05	0.25	0.16	-0.36^{*}	-0.06	85.43
m_l	0.13	-0.39	-0.10	-0.64	0.39	0.04	0.04	-0.05	0.05	74.76
S—i	-0.25	0.22	0.34	0.41	-0.25	-0.00	-0.17	0.50^{**}	0.33^{*}	84.29
Node 6 (STH) of Element 1: 1st p.v.	-0.48	0.52^{***}	0.01	0.18	-0.13	0.55^{***}	-0.03	-0.07	0.08	86.89
a-p	0.66^{***}	-0.35	-0.12	0.31	-0.22	0.28	-0.02	0.22	-0.11	85.16
m_l	0.08	-0.47	-0.04	-0.66^{*}	0.02	0.11	0.01	0.21	0.42^{**}	89.63
S—i	-0.73^{***}	0.13	0.10	0.17	0.41^{*}	0.04	-0.09	-0.27^{*}	0.04	84.53
Node 3 (i) of Element 2: 1st p.v.	-0.29	-0.66^{***}	-0.24^{***}	0.13^{*}	-0.36^{***}	0.17^{**}	0.17^{**}	0.15^{**}	-0.02	80.11
a-b	0.55^{**}	0.15	0.03	0.29	0.40	0.20	-0.31	0.00	-0.32	79.74
m_l	-0.07	-0.33	-0.01	-0.22	0.23	0.64^{**}	-0.41	0.09	0.25	85.89
S-i	-0.32	-0.25	0.20	-0.09	-0.67^{*}	-0.22	0.44^{*}	-0.08	-0.08	91.40
Node 8 (SCH) of Element 2: 1st p.v.	-0.66^{**}	-0.26	-0.10	-0.17	0.22^{*}	0.30^{**}	0.11	0.30^{*}	-0.39^{**}	93.07
a-p	-0.59^{***}	-0.35	-0.04	0.27	0.25	-0.44^{**}	-0.18	-0.08	0.16	86.00
m-l	0.12	-0.32	-0.31	0.21	-0.25	0.34	0.32	-0.39	0.29	77.66
S-i	0.44^{*}	0.68	0.16	-0.32	-0.10	0.31	0.05	-0.07	-0.02	89.66
Node 1 (g) of Element 3: 1st p.v.	-0.06	-0.06	0.80^{***}	-0.05	-0.18	0.26^{*}	-0.10	-0.24^{*}	-0.01	81.21
a-p	-0.16	-0.25	-0.72^{*}	0.31	0.05	0.13	-0.31	0.08	0.04	82.27
m_l	-0.25	0.39	-0.48	-0.51	-0.07	-0.00	0.02	-0.30	-0.10	79.80
S-i	0.23	-0.06	0.76^{*}	0.24	0.19	0.13	0.14	0.00	0.15	78.54
Node 7 (zm) of Element 3: 1 st p.v.	-0.25	-0.39^{***}	0.46^{***}	-0.40^{***}	-0.11^{*}	0.18^{**}	-0.18^{**}	-0.24^{***}	-0.13^{*}	74.21
ap	0.13	-0.35	0.06	0.42	0.50^{*}	0.06	0.49^{*}	0.05	-0.01	81.83
m-l	-0.06	-0.46	0.09	0.03	-0.62	0.10	-0.43	0.08	-0.30	89.05
S—i	0.41^{*}	0.53	-0.33	-0.19	-0.27	0.03	0.07	0.29	0.11	76.32
Age	-0.31	0.08	0.12	-0.21	0.26	0.30	0.49	0.48^{*}	-0.17	81.66
Total contribution (%)	15.58	14.37	11.07	10.15	9.21	7.72	6.25	5.59	3.71	83.64
Cumulative proportion (%)	15.58	29.95	41.02	51.17	60.37	68.09	74.34	79.93	83.64	83.64

² p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction cosine for the superior-inferior axis. * P < 0.05; ** P < 0.01; *** P < 0.001, by a two-tailed bootstrap test.

at six craniotacial landmarks, i.e	e., tt, STH, 1, SC	H, g, and zm II	n the three left	elements, and	age 1n African-/	Americans. ¹			
Vorrighla ²					Factor loadings				
VallaUIC	Fac I	Π	III	IV	Λ	VI	VII	VIII	IX
Node 5 (ft) of Element 1: 1 st p.v.	0.04	-0.02	-0.14	0.16	-0.11	0.92^{***}	0.05	-0.01	-0.13
a-p	0.83^{***}	0.06	0.06	-0.03	0.22	-0.21	-0.05	-0.20	0.16
m-l	0.03	-0.04	0.02	-0.56	0.02	-0.40^{*}	0.14	-0.46^{**}	-0.18
S-i	-0.28	-0.02	0.06	0.06	-0.09	0.23	-0.07	0.83^{***}	0.02
Node 6 (STH) of Element 1: 1st p.v.	-0.14	0.10	0.06	-0.00	0.01	0.90^{***}	0.01	0.11	-0.10
a-p	0.63^{***}	0.33	-0.11	-0.00	0.25	-0.28	-0.35	0.28	0.02
m-l	0.02	0.10	-0.01	-0.80	-0.31	-0.37	0.01	-0.07	-0.08
S-i	-0.27	-0.65^{***}	0.12	0.01	0.07	0.51^{**}	0.22	-0.10	-0.11
Node 3 (i) of Element 2: 1st p.v.	0.42	-0.28	-0.23	-0.16	-0.44	0.01	-0.44	0.11	-0.25
a-p	0.17	0.16	0.04	0.15	0.84^{***}	-0.10	-0.01	0.01	0.04
m_l	0.11	-0.09	0.07	-0.81^{**}	0.29	0.20	-0.20	0.04	-0.10
s-i	0.07	-0.03	0.22	0.26	-0.84^{***}	-0.03	-0.28	-0.01	-0.09
Node 8 (SCH) of Element 2: 1st p.v.	-0.15	-0.35	-0.10	-0.18	-0.06	0.21	-0.24	-0.16	-0.78^{***}
a-p	-0.18	-0.87^{***}	-0.16	0.01	-0.14	-0.04	0.04	0.11	0.08
m-l	0.75^{***}	0.00	-0.10	-0.13	-0.29	0.24	0.02	-0.09	0.20
S-i	-0.16	0.81^{*}	0.26	0.02	0.20	0.20	0.19	-0.15	0.10
Node 1 (g) of Element 3: 1st p.v.	-0.03	-0.01	0.85^{***}	-0.08	-0.04	0.14	-0.21	0.11	0.07
a-p	0.23	-0.30	-0.72^{**}	-0.16	0.18	0.20	-0.25	0.03	0.06
m-l	-0.32	0.20	-0.31	-0.05	-0.18	0.31	0.08	-0.64^{***}	0.06
S—i	0.18	-0.03	0.71^{***}	0.02	0.17	-0.12	0.22	0.39^{*}	-0.04
Node 7 (zm) of Element 3: 1st p.v.	-0.10	-0.22	0.57	-0.34	-0.16	-0.04	-0.38	-0.26	-0.06
a-p	0.57^{*}	-0.32	0.07	0.13	0.16	-0.19	0.39	0.15	-0.37
m_l	0.04	-0.06	0.07	-0.05	-0.14	-0.08	-0.91^{***}	0.10	0.09
S-i	-0.13	0.76	-0.37	0.04	-0.01	0.01	0.12	0.08	0.10
Age	-0.10	0.11	0.07	- 0.09	-0.10	0.11	0.21	0.06	-0.84^{***}
¹ The sample size is 27. The cumul	ative proportion	n of the variance	es of the nine p	rincipal compo	onents is 83.64%	<u>0</u> .			
² p.v.: principal value; a-p: direction	n cosine for the	anterior-posterio	or axis; m–l: dir	rection cosine f	or the medial-la	teral axis; s-i: d	irection cosine	for the superior-	inferior axis.
$^{*}P < 0.05; ^{**}P < 0.01; ^{**}P < 0.01$	001, by a two-ta	iled bootstrap to	est.					4	

Table 13. Rotated solution of the first nine principal components extracted from the correlations between the linearized first principal values and their direction cosines

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VZ-11-2					ц	actor loading			1			otal variance
variable	PC I	П	Ш	N	>	IV	ПΛ	VIII	IX	×	IX	(%)
Node 3 (b) of Element 1: 1st p.v.	-0.05	0.84^{***}	0.03	0.16^{**}	0.19^{**}	-0.15^{*}	0.18^{**}	- 0.06	0.07	0.19^{***}	0.07	87.56
a-p	0.26	-0.45	0.18	-0.37	0.02	-0.14	-0.22	-0.43^{*}	-0.08	-0.15	0.16	74.11
m_l	-0.03	0.09	-0.28	-0.04	-0.33	0.05	0.24	-0.00	-0.71^{***}	-0.18	-0.26	86.53
S-i	0.07	-0.32	0.12	0.26	-0.31	0.38	0.11	0.57^{*}	0.38^{*}	0.08	0.11	93.03
Node 4 (ba) of Element 1: 1st p.v.	-0.22	0.82^{***}	0.17^{***}	-0.02	0.04	-0.04	-0.16^{***}	-0.05	0.03	0.16^{***}	0.14^{***}	83.02
a-p	-0.76^{***}	-0.17	0.29	-0.06	-0.24	0.12	-0.08	-0.25^{*}	0.04	0.07	-0.25^{**}	89.96
m-l	0.37^{*}	0.05	0.06	-0.59^{*}	0.02	-0.32	-0.02	0.15	0.19	-0.07	0.16	68.60
S-i	0.25	-0.08	0.04	0.68^{*}	0.18	0.10	-0.03	0.18	-0.12	-0.24	0.46^{***}	88.19
Node 4 (1) of Element 2: 1st p.v.	0.03	0.60^{***}	-0.39^{***}	-0.00	0.09^{*}	0.27^{***}	-0.25^{***}	-0.14^{**}	0.21^{***}	-0.14^{**}	-0.17^{***}	77.12
a-p	-0.06	0.10	0.58	-0.13	-0.03	0.42	0.21	-0.29	0.14	-0.31	-0.07	78.48
m-l	-0.34^{*}	0.12	-0.07	0.23	0.04	-0.65^{**}	0.44	-0.17	-0.09	-0.03	0.17	86.33
Si	0.46^{**}	-0.27	-0.41	0.24	-0.10	-0.10	-0.41^{*}	-0.23	0.06	0.06	-0.08	76.58
Node 7 (ast) of Element 2: 1st p.v.	-0.18	0.05	0.01	-0.46^{***}	0.41^{***}	0.34^{***}	-0.33^{***}	0.34^{***}	-0.33^{***}	-0.05	-0.10^{**}	87.39
a-p	0.40^{*}	0.24	0.12	-0.11	0.65^{**}	-0.13	-0.16	0.32	-0.10	-0.19	-0.13	87.35
m-l	0.02	-0.07	-0.05	-0.43	-0.05	0.54^{**}	0.25	-0.08	-0.24	0.31	0.41^{**}	87.35
S-i	-0.51^{***}	-0.30	-0.21	-0.17	-0.16	-0.44^{*}	-0.16	0.30	0.24	-0.19	-0.14	86.68
Node 2 (fmt) of Element 3: 1st p.v.	-0.39	0.14^{*}	-0.36^{***}	0.12^{**}	0.05	0.22^{***}	-0.44^{***}	-0.36^{***}	0.16^{***}	-0.24^{***}	0.27^{***}	83.79
a-p	-0.24	0.44	0.35	-0.23	-0.51^{*}	-0.17	-0.26	0.30	-0.05	0.11	0.02	88.58
m-l	0.59^{***}	0.06	0.05	-0.21	0.24	0.06	0.48^{*}	-0.12	0.27	-0.21	-0.25	87.88
S-1	-0.52^{***}	-0.36	-0.25	0.03	0.61^{**}	-0.09	-0.01	0.05	-0.18	0.16	0.06	90.28
Node 5 (n) of Element 3: 1st p.v.	-0.56^{**}	-0.05	0.47***	-0.16	0.16	-0.06	0.02	0.04	0.02	-0.48^{***}	0.22^{**}	87.42
a-p	0.59^{***}	0.24	-0.16	-0.19	-0.47^{*}	-0.09	-0.17	0.01	-0.14	-0.20	0.12	80.18
m-l	0.25	-0.20	0.61	0.09	0.28	-0.09	-0.26	-0.19	0.05	0.42^{**}	-0.16	88.22
S-i	-0.35^{*}	0.05	-0.64	-0.19	0.16	0.24	0.25	0.05	0.28	0.01	-0.10	80.45
Occlusal wear of UM1	-0.03	0.09	0.29	0.68^{***}	-0.01	0.18	-0.09	0.06	-0.17	-0.19	-0.27^{*}	73.27
Total contribution (%)	13.48	11.15	9.52	9.14	8.10	7.20	6.17	5.64	5.12	4.37	4.05	83.93
Cumulative proportion (%)	13.48	24.63	34.15	43.29	51.38	58.59	64.75	70.40	75.52	79.89	83.93	83.93
¹ The sample size is 33. The	number of pr	incipal con	nponents she	own here w	as determir	ned so that t	he cumulati	ve proporti	on of the va	riances of t	he principal	components

exceeded 80%.

² p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction cosine for the superior-inferior axis.

* P < 0.05; ** P < 0.01; *** P < 0.001, by a two-tailed bootstrap test.

V.C2					Fa	actor loading	ŝ				
VALIADIC	Fac I	П	III	IV	>	ΙΛ	ΠΛ	VIII	IX	Х	IX
Node 3 (b) of Element 1: 1st p.v.	00.0	0.91***	-0.02	0.01	0.11	-0.11	0.00	-0.15	-0.00	-0.00	0.08
a-p	0.16	-0.57^{**}	-0.09	-0.32	0.04	-0.02	0.09	-0.36^{*}	0.36	0.11	0.01
m-l	0.22	-0.11	0.28	0.35	-0.09	0.07	-0.11	-0.40^{**}	-0.62^{***}	0.16	-0.11
S-i	0.07	-0.19	0.13	0.11	-0.05	-0.05	0.01	0.91^{***}	-0.03	0.05	0.13
Node 4 (ba) of Element 1: 1st p.v.	0.15	0.82^{**}	-0.19	-0.02	-0.20	0.07	0.15	-0.14	0.09	0.03	-0.06
a-p	-0.20	-0.11	-0.12	0.30	-0.35	-0.15	0.45^{*}	0.01	0.09	-0.01	-0.62^{***}
m-l	0.27	-0.02	0.16	-0.73^{***}	0.15	0.15	0.02	-0.05	0.07	-0.08	0.01
S-i	-0.02	-0.05	-0.06	0.30	-0.02	-0.08	-0.02	0.16	0.05	-0.00	0.87^{***}
Node 4 (1) of Element 2: 1st p.v.	0.16	0.44	-0.59	0.08	0.21	0.24	-0.20	-0.04	-0.20	-0.07	-0.11
a-p	0.23	-0.01	-0.10	0.21	0.36^{*}	-0.01	0.66^{***}	0.05	0.19	0.22	-0.17
m_l	-0.31	0.25	0.23	-0.08	-0.10	-0.59^{***}	0.15	-0.38	-0.20	-0.24	0.13
S-i	0.16	-0.35	-0.29	0.03	0.03	-0.08	-0.67^{***}	-0.08	0.16	-0.15	0.13
Node 7 (ast) of Element 2: 1st p.v.	-0.19	-0.01	-0.04	-0.07	-0.14	0.86^{***}	0.15	-0.07	-0.07	0.15	-0.08
a-p	-0.03	0.21	0.16	-0.16	0.34	0.63^{***}	-0.03	-0.17	0.18	-0.26	0.37^{*}
m_l	-0.04	-0.07	0.03	-0.20	-0.03	0.10	0.06	0.07	-0.12	0.89^{***}	-0.07
S—i	-0.23	-0.24	-0.01	-0.29	-0.37	-0.05	0.12	0.13	-0.28	-0.59^{***}	-0.28
Node 2 (fmt) of Element 3: 1st p.v.	-0.12	0.03	-0.86^{***}	0.07	-0.23	-0.03	0.07	-0.10	-0.11	0.00	0.04
a-p	0.47	0.38	0.17	-0.11	-0.56^{**}	0.09	0.23	0.11	0.00	-0.11	-0.28
m-l	0.16	-0.02	0.16	-0.18	0.89^{***}	0.00	-0.01	-0.01	0.02	0.01	0.02
S-i	-0.88^{***}	-0.13	-0.03	-0.02	-0.20	0.16	0.01	-0.17	-0.05	-0.02	0.06
Node 5 (n) of Element 3: 1st p.v.	-0.16	-0.05	-0.06	-0.06	-0.18	0.06	0.88^{***}	-0.07	0.00	-0.16	0.05
a-p	0.77^{***}	-0.05	-0.01	-0.23	0.00	0.03	-0.28	-0.13	-0.17	0.04	0.16
m_l	-0.06	-0.04	0.22	0.10	0.05	0.08	-0.05	-0.06	0.90^{***}	0.00	-0.05
S—i	-0.45	0.10	-0.33	-0.15	0.20	0.03	-0.11	0.18	-0.54^{***}	0.06	-0.29^{*}
Occlusal wear of UM1	0.09	0.07	0.04	0.77^{**}	-0.01	0.03	0.09	0.08	0.11	-0.22	0.22
¹ The sample size is 33. The cum	ulative propoi	rtion of the v	ariances of t	he eleven pri	ncipal comp	onents is 83	93%.				
² n v · nrincinal value· a–n· directi	ion cosine for	the anterior-r	osterior axis	· m—l· directi	on cosine for	the medial-	lateral axis: s	-i- direction	cosine for the	e superior-in	ferior axis
							· · · · · · · · · · · · · · · · · · ·			to to the day of	
P < 0.05; P < 0.01; P < 0.01; P < 0.01	0.001, by a tw	o-tailed boot	tstrap test.								

e 15. Rotated solution of the first eleven principal components extracted from the correlations between the linearized first principal values and their direction cosines at six craniofacial landmarks. i.e., b, ba, l, ast, fint, and n in the three right elements, and the degree of occlusal wear on the maxillary first molar in early

Table 15.

Variable					Fa	ictor loadings	S					Total
	PC I	Π	III	IV	>	ΙΛ	ΠΛ	VIII	IX	х	XI	variance (%)
Node 3 (b) of Element 1: 1st p.v.	-0.49^{*}	0.45***	0.21**	0.24***	-0.31^{***}	0.17^{***}	0.21***	-0.09^{*}	0.32^{***}	0.06	-0.10^{*}	84.53
a-p	0.52^{***}	0.27	0.04	-0.37	-0.41	-0.01	-0.31	0.04	-0.10	0.03	-0.18	79.04
m_l	-0.10	0.24	0.48^{*}	0.16	0.51	-0.19	0.18	-0.29	0.03	-0.03	-0.21	77.50
S-i	0.02	-0.18	-0.24	0.45	-0.02	0.07	0.51^{*}	0.33	-0.05	-0.02	0.49^{***}	90.12
Node 4 (ba) of Element 1: 1st p.v.	0.37	0.35^{***}	0.02	-0.06	-0.42^{***}	0.43^{***}	0.11^{***}	-0.04	0.11^{***}	-0.10^{***}	0.27^{***}	72.45
a-p	0.33	0.29	-0.39	-0.13	0.14	-0.48^{*}	0.22	0.20	0.21	-0.22	0.08	80.08
m-l	0.65^{***}	0.11	0.25	0.26	0.18	0.15	0.12	0.16	-0.09	0.12	0.13	69.46
Si	-0.63^{***}	-0.11	0.13	0.07	-0.36	0.35	-0.18	-0.05	-0.18	0.16	0.23	82.99
Node 4 (1) of Element 2: 1st p.v.	-0.24	0.30^{***}	-0.09	-0.11^{*}	-0.01	0.52^{***}	0.16^{***}	0.14^{***}	0.43^{***}	-0.46^{***}	-0.15^{***}	90.06
a-p	0.16	-0.01	0.62	-0.13	-0.27	-0.24	-0.17	0.24	-0.38	-0.27	0.13	87.64
m_l	0.05	0.13	-0.07	0.68^{**}	-0.16	-0.53^{*}	0.14	-0.05	0.02	0.11	-0.12	84.74
S-i	0.22	-0.45	-0.23	-0.29	0.39	0.50	-0.03	-0.13	-0.08	0.15	0.10	84.27
Node 7 (ast) of Element 2: 1st p.v.	0.29	-0.13^{*}	-0.11^{*}	-0.49^{***}	0.08	0.19^{***}	0.46^{***}	0.26^{***}	-0.12^{*}	0.01	-0.33^{***}	79.92
a-p	-0.27	0.29	-0.47	-0.07	-0.40	-0.12	0.27	-0.38^{*}	-0.31	-0.19	0.01	91.50
m-l	0.46^{**}	-0.31	0.49	0.33	0.23	0.18	0.06	-0.16	0.24	-0.06	0.07	84.57
Si	-0.21	0.22	-0.20	-0.03	-0.00	-0.08	-0.54	0.32	0.37	0.39^{*}	0.06	82.59
Node 2 (fmt) of Element 3: 1st p.v.	0.51^{*}	0.21^{***}	-0.05	0.23^{***}	-0.11^{**}	0.08	-0.50^{***}	-0.22^{***}	0.12^{***}	-0.38^{***}	0.13^{***}	84.57
a-p	0.41^{**}	-0.03	0.05	-0.49	-0.12	-0.37	0.06	-0.34	0.34^{*}	0.17	0.22	87.00
m-l	0.11	-0.50	0.23	0.26	-0.47	0.00	-0.04	0.38^{*}	0.05	-0.14	-0.32^{*}	87.58
S—i	-0.26	0.35	-0.05	0.23	0.53^{*}	0.20	-0.33	0.00	-0.21	-0.19	-0.05	76.11
Node 5 (n) of Element 3: 1st p.v.	-0.08	0.72^{***}	0.40^{***}	-0.24	0.22^{*}	-0.06	0.06	0.04	-0.16^{*}	-0.09	0.18^{***}	86.57
a-p	-0.06	-0.60	-0.39	0.07	0.06	-0.13	-0.18	-0.30	-0.03	-0.32^{*}	-0.00	76.58
m-l	-0.55^{***}	-0.16	0.44	-0.47	0.01	-0.20	0.17	-0.01	0.09	-0.05	0.15	84.60
S—i	0.39^{*}	0.63	-0.25	0.18	-0.03	0.23	0.08	-0.08	-0.22	0.30^{*}	-0.15	86.91
Occlusal wear of UM1	0.18	-0.21	0.31^{*}	0.10	-0.32^{**}	0.22	0.19	-0.44^{***}	0.04	0.14	-0.10	60.13
Total contribution (%)	12.53	11.63	9.02	8.75	8.10	7.69	69.9	5.25	4.50	4.27	3.63	82.06
Cumulative proportion (%)	12.53	24.15	33.18	41.93	50.03	57.72	64.41	69.66	74.16	78.43	82.06	82.06

exceeded 80%. 2 p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction cosine for the superior-inferior 2 p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the superior-inferior axis. * P < 0.05; ** P < 0.01; *** P < 0.001, by a two-tailed bootstrap test.

15					Fs	actor loading	SS				
Variable	Fac I	Π	III	IV	>	IV	ΝII	VIII	IX	x	XI
Node 3 (b) of Element 1: 1st p.v.	0.02	0.19	-0.10	0.56	-0.01	0.39	0.12	0.06	0.54^{*}	0.13	0.02
a-p	0.46	-0.11	-0.11	-0.13	-0.43^{*}	-0.13	-0.11	0.12	0.02	-0.44^{*}	0.33
m_l	-0.16	0.51^{*}	0.37	0.33	-0.25	-0.07	0.12	-0.32	-0.05	0.11	-0.21
S-i	0.05	-0.13	0.04	0.07	0.92^{***}	-0.06	0.07	-0.09	0.00	0.08	-0.04
Node 4 (ba) of Element 1: 1st p.v.	0.48^{*}	0.07	-0.02	-0.11	0.17	0.11	-0.23	-0.07	0.46	-0.21	0.35
a-p	0.06	0.11	-0.16	0.12	0.16	-0.82^{***}	-0.05	0.11	0.04	0.01	0.15
m-l	0.49	0.08	0.55^{*}	-0.05	0.22	-0.15	-0.03	-0.13	-0.10	-0.19	0.03
S-i	-0.18	-0.03	-0.26	-0.01	0.14	0.82^{***}	0.00	0.15	0.07	-0.07	-0.09
Node 4 (l) of Element 2: 1st p.v.	-0.05	0.02	-0.06	-0.09	-0.02	-0.05	-0.01	0.00	0.91^{***}	0.12	-0.18
a-p	-0.12	-0.00	0.11	0.08	-0.07	0.06	-0.06	-0.12	-0.15	-0.89^{***}	0.04
m_l	0.16	-0.15	0.01	0.79^{***}	0.17	-0.15	-0.08	-0.06	-0.30	0.13	-0.04
S-i	0.05	-0.05	0.18	-0.81^{***}	0.04	0.08	0.03	-0.10	-0.12	0.33	-0.00
Node 7 (ast) of Element 2: 1st p.v.	0.17	-0.16	-0.02	-0.43	-0.07	-0.34	0.58^{*}	-0.24	0.16	-0.06	0.11
a-p	0.12	0.09	-0.86^{***}	0.17	0.06	0.02	-0.07	-0.30	0.06	0.10	0.07
m_l	0.00	-0.07	0.81^{***}	-0.02	0.06	0.04	-0.22	-0.34	-0.01	0.04	0.11
Si	0.02	0.01	-0.01	0.09	-0.13	0.05	-0.05	0.88^{***}	0.01	0.12	-0.02
Node 2 (fmt) of Element 3: 1st p.v.	0.31	-0.06	0.14	-0.00	-0.15	-0.15	-0.81^{***}	-0.00	0.10	-0.13	0.02
a-p	-0.08	0.18	0.04	-0.10	-0.19	-0.28	-0.11	0.02	-0.15	0.02	0.82^{***}
m_l	-0.08	-0.80^{***}	0.23	0.19	0.01	0.12	0.09	-0.07	0.06	-0.32	0.00
S-i.	0.05	0.37^{*}	0.03	-0.04	-0.11	0.04	-0.21	0.10	0.04	0.10	-0.74^{***}
Node 5 (n) of Element 3: 1st p.v.	0.08	0.78^{**}	-0.00	0.11	-0.10	-0.07	0.09	0.03	0.19	-0.40	-0.10
a-p	-0.38^{***}	-0.41^{*}	-0.19	-0.21	0.01	-0.09	-0.39^{*}	-0.21	-0.27	0.30^{*}	-0.09
m_l	-0.72^{*}	0.28	-0.07	-0.01	-0.08	0.20	0.33^{*}	-0.01	0.09	-0.21	0.20
S-i	0.88^{***}	0.24	-0.10	0.09	-0.05	-0.06	0.03	-0.01	0.02	0.11	-0.05
Occlusal wear of UM1	0.13	-0.14	0.20	0.08	-0.12	0.39	-0.02	-0.44	0.01	0.09	0.38
¹ The sample size is 33. The cumu	ulative propor	tion of the va	triances of th	ie eleven pri	ncipal comp	onents is 82	.06%.				
* <i>P</i> < 0.05: ** <i>P</i> < 0.01: *** <i>P</i> < 0.01	on cosine for t 001, by a two	the anterior-po o-tailed boots	osterior axis; tran test	m-l: directi	on cosine for	r the medial-	lateral axis;	s-i: direction o	cosine for th	e superior-ir	ferior axis.

Table 17. Rotated solution of the first eleven principal components extracted from the correlations between the linearized first principal values and their direction cosines at six cranicferial landmarks i.e. b. ba 1 act fint and n in the three left elements and the degree of occlused war on the maxillary first molar in early mod-

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able 18. Principal component analysis of the correlations	ba. I. ast. fmt. and n in the three right elements, and the d

	0	6			Factor 1	oadings					Total
Variable ²	PC I	П	III	IV	>	IV	ΠΛ	IIIA	IX	x	variance (%)
Node 3 (b) of Element 1: 1st p.v.	0.34	0.32	0.58	0.05	-0.24	0.31	- 0.21	0.06	0.02	- 0.18	79.09
a-p	0.55	0.03	-0.05	-0.12	0.63^{*}	-0.27	-0.09	0.08	0.07	0.19	85.54
m-l	-0.43	-0.03	0.47	0.01	0.31	-0.18	0.05	0.41	0.28	0.05	79.27
S-i	-0.37	-0.23	-0.21	-0.17	-0.49	0.32	0.21	-0.43	-0.09	0.13	86.35
Node 4 (ba) of Element 1: 1st p.v.	-0.09	0.58	0.47	-0.21	-0.02	0.44	-0.16	-0.04	0.02	0.10	84.72
a-p	0.40	0.11	-0.51	-0.18	-0.10	-0.01	-0.61^{*}	-0.11	-0.02	0.23	90.89
m-l	-0.52	0.18	0.37	-0.09	-0.10	-0.60^{*}	0.17	-0.10	0.14	-0.19	90.90
S-i	0.14	-0.38	0.12	0.43	0.22	0.42	0.12	0.41	-0.10	0.15	80.75
Node 4 (I) of Element 2: 1st p.v.	-0.04	0.57	0.44	0.48	-0.14	0.16	-0.01	0.04	-0.06	0.08	80.57
a-p	0.06	-0.74	0.25	-0.17	-0.16	0.31	-0.04	0.10	0.21	0.14	84.38
m-l	0.60	-0.01	-0.01	-0.07	-0.08	-0.54	-0.11	0.24	-0.05	-0.11	74.91
S-i	-0.32	0.52	-0.25	-0.33	0.24	-0.04	-0.04	-0.06	0.05	0.16	64.34
Node 7 (ast) of Element 2: 1st p.v.	0.16	0.20	0.66	0.32	0.22	-0.09	-0.04	-0.44^{*}	-0.10	0.07	87.57
a-p	0.09	0.43	-0.32	0.41	-0.24	-0.07	0.43	0.05	0.14	0.09	74.10
m-l	0.06	-0.43	0.23	0.27	-0.37	-0.38	-0.27	-0.26	-0.33	-0.07	85.21
S-i	0.08	0.12	0.21	-0.76^{*}	0.33	0.09	0.06	-0.16	-0.21	-0.01	83.66
Node 2 (fmt) of Element 3: 1st p.v.	-0.44	0.20	-0.05	0.23	0.18	-0.17	-0.11	0.15	-0.56^{*}	0.43	87.38
a-p	0.66	0.45	-0.13	0.05	00.00	0.13	-0.10	-0.11	0.25	-0.25	81.74
m_l	-0.16	-0.49	0.55	-0.23	0.35	-0.02	-0.09	-0.25	0.15	0.06	84.32
S-i	-0.39	-0.00	0.02	-0.47	-0.52	-0.05	-0.13	0.42^{*}	-0.02	-0.09	84.76
Node 5 (n) of Element 3: 1st p.v.	-0.56	0.36	-0.11	-0.13	0.04	0.16	-0.38	0.18	-0.05	-0.14	69.00
ap	0.60	-0.16	0.16	-0.22	0.03	0.19	0.17	0.21	-0.47^{*}	-0.19	82.03
m-l	0.47	0.11	0.13	-0.28	-0.34	-0.10	0.26	-0.01	0.32	0.48^{*}	85.06
s-i	-0.28	-0.30	-0.27	0.43	0.24	0.15	-0.45	-0.11	0.33	-0.06	83.92
Occlusal wear of UM1	-0.16	0.04	-0.40	-0.04	0.54	0.21	0.36	-0.14	-0.09	-0.25	74.42
Total contribution (%)	14.04	12.02	11.22	9.07	8.85	7.20	5.78	5.21	4.81	3.61	81.79
Cumulative proportion (%)	14.04	26.06	37.28	46.35	55.19	62.39	68.17	73.38	78.19	81.79	81.79
¹ The sample size is 35. The nurr	nber of princ	ipal compor	ients shown]	here was det	termined so	that the cum	ulative prop	ortion of the	variances o	f the princi	oal components

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exceeded 80%.

²p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction cosine for the superior-inferior axis.

* P < 0.05; ** P < 0.01; *** P < 0.001, by a two-tailed bootstrap test.

at six craniofacial landmarks, i.	ı.e., b, ba, l, ast	, timt, and n in	the three rig	ht elements, a	nd the degree	of occlusal w	ear on the may	killary first m	olar in Indians	
Voriabla ²					Factor	loadings				
VallaDIC	Fac I	П	III	N	>	ΙΛ	IIA	VIII	IX	x
Node 3 (b) of Element 1: 1st p.v.	0.04	-0.09	0.80^{*}	-0.03	0.10	-0.14	0.17	0.04	0.27	0.05
a-p	0.20	-0.04	-0.18	-0.19	0.72^{***}	0.22	0.10	-0.37	-0.02	0.17
m_l	-0.70^{**}	-0.07	0.11	-0.26	0.27	0.16	-0.25	0.18	-0.17	0.03
S—i	0.12	0.08	-0.17	-0.03	-0.89^{***}	-0.05	0.01	0.09	0.00	0.10
Node 4 (ba) of Element 1: 1 st p.v.	0.00	0.12	0.80^{*}	-0.15	-0.12	0.36^{*}	0.09	0.08	-0.06	0.06
a-p	0.89^{***}	0.15	-0.07	-0.01	0.21	-0.01	-0.14	0.12	-0.04	0.12
m_l	-0.68^{**}	0.63^{***}	0.02	-0.03	-0.00	-0.16	-0.08	0.11	-0.09	0.01
S-i	-0.11	-0.87^{***}	0.02	-0.01	0.06	-0.02	-0.02	-0.11	-0.10	-0.08
Node 4 (l) of Element 2: 1st p.v.	-0.19	-0.03	0.76^{**}	0.36	-0.01	-0.05	-0.08	-0.15	-0.19	-0.01
a-p	-0.05	-0.52	-0.13	-0.54^{*}	-0.22	-0.20	-0.07	0.18	0.26	0.28
m_l	0.15	0.11	-0.14	0.12	0.64^{**}	-0.36	0.26	0.08	0.15	0.20
s-i	0.08	0.45^{*}	0.02	0.04	0.01	0.58^{**}	-0.08	0.09	-0.27	-0.03
Node 7 (ast) of Element 2: 1st p.v.	-0.20	0.13	0.53	-0.17	0.10	-0.24	0.02	-0.66^{***}	-0.10	0.03
a-p	-0.06	0.03	-0.01	0.82^{***}	-0.06	0.11	-0.06	-0.14	0.01	0.18
m_l	0.04	0.08	-0.05	-0.14	-0.08	-0.89^{***}	0.00	-0.08	-0.11	-0.05
S—I.	0.06	0.28	0.05	-0.54	0.03	0.41	0.54^{**}	-0.03	-0.00	0.03
Node 2 (fint) of Element 3: 1st p.v.	-0.04	0.02	0.02	0.11	0.00	0.01	-0.04	0.00	-0.91^{***}	-0.16
a-p	0.41	0.10	0.30	0.32	0.33	0.15	0.08	-0.21	0.51^{*}	0.04
m-l	-0.33	-0.03	-0.02	-0.82^{***}	-0.03	-0.07	-0.09	-0.23	0.05	0.06
S-i	-0.12	0.17	0.03	-0.08	-0.17	-0.05	0.09	0.87^{***}	-0.05	0.07
Node 5 (n) of Element 3: 1st p.v.	0.03	0.23	0.24	-0.03	-0.08	0.30	-0.24	0.45	-0.24	-0.41
a-p	0.18	-0.35^{*}	0.04	-0.10	0.18	-0.12	0.76^{***}	-0.03	0.15	-0.04
m_l	0.09	0.05	0.08	0.08	0.04	0.04	0.18	-0.01	0.17	0.87^{***}
S—i	0.14	-0.20	-0.15	-0.13	-0.02	-0.03	-0.78^{***}	-0.09	0.05	-0.36
Occlusal wear of UM1	-0.05	-0.02	-0.37	0.08	-0.11	0.53^{**}	0.12	-0.30	0.05	-0.45^{*}
¹ The sample size is 35. The cumu	ulative proport	ion of the vari	ances of the	ten principal c	omponents is	81.79%.				
² p.v.: principal value; a–p: directic	on cosine for th	ne anterior-pos	terior axis; m	-l: direction co	osine for the n	nedial-lateral a	xis; s–i: direct	ion cosine for	the superior-i	nferior axis.
*P < 0.05; **P < 0.01; ***P < 0.01	001, by a two	-tailed bootstr	ap test.				~			

Rotated solution of the first ten principal components extracted from the correlations between the linearized first principal values and their direction cosines

Table 19.

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Node 3 (b) of Element 1: 1st p.v.	0.29	0.71	-0.33	0.14	0.21	0.05	0.18	-0.12	0.05	0.01	0.16	82.99
a-p	0.51	-0.52	0.12	0.22	0.14	-0.30	-0.01	-0.17	-0.27	0.01	-0.07	81.00
m-l	0.11	0.30	-0.10	-0.04	-0.25	-0.38	-0.33	-0.24	0.32	-0.36	0.17	74.28
S-i	-0.67	0.33	-0.05	-0.17	0.02	0.39	0.26	0.06	0.15	0.03	0.32^{*}	93.19
Node 4 (ba) of Element 1: 1st p.v.	0.46	0.61	-0.12	0.29	0.10	0.09	-0.01	-0.29	-0.07	0.22	0.12	85.21
a-p	-0.04	-0.06	-0.29	0.23	-0.18	-0.33	0.28	0.51	0.15	0.36	0.34	88.13
m_l	0.57	-0.06	0.43	0.41	0.01	0.32	0.10	-0.15	-0.06	-0.13	-0.03	83.80
S-1.	-0.51	0.05	-0.28	-0.33	0.33	0.22	-0.10	-0.43^{*}	0.12	0.03	-0.08	82.61
Node 4 (l) of Element 2: 1 st p.v.	0.25	0.61	-0.13	-0.33	-0.31	-0.03	-0.18	-0.09	0.18	-0.02	-0.33^{*}	84.11
a-p	0.06	-0.20	-0.15	-0.40	0.66^{*}	0.16	0.31	0.12	-0.01	-0.01	-0.04	79.14
m-l	-0.27	0.05	-0.34	0.36	0.30	-0.25	-0.28	-0.07	-0.36	-0.01	0.25	75.29
Si	0.18	0.01	0.64	0.06	-0.12	0.36	0.05	0.16	0.46^{*}	0.01	0.11	84.72
Node 7 (ast) of Element 2: 1st p.v.	0.67	0.38	-0.16	-0.19	0.05	0.03	0.27	0.03	-0.05	0.18	0.01	75.55
a-p	0.01	-0.11	0.16	0.43	0.30	0.02	-0.39	0.05	0.38	0.40	-0.01	77.43
m-l	0.44	-0.12	-0.18	-0.46	0.12	0.20	-0.19	0.03	-0.07	-0.34	0.49^{*}	90.62
S-i	-0.59	0.24	0.11	0.20	-0.17	-0.30	0.39	-0.22	0.04	-0.08	-0.20	82.46
Node 2 (fmt) of Element 3: 1st p.v.	-0.04	0.33	-0.07	0.09	0.29	-0.38	-0.32	0.52^{*}	0.11	-0.30	-0.13	84.36
a-p	-0.08	-0.32	-0.34	0.16	-0.60	0.26	-0.34	0.08	0.07	-0.07	0.13	82.91
m-l	0.34	-0.02	-0.17	-0.56	0.18	-0.20	-0.29	0.12	0.22	0.33	-0.15	81.55
S-i	-0.06	0.36	0.28	0.38	0.53	0.09	0.03	0.32	0.08	-0.36	-0.09	89.26
Node 5 (n) of Element 3: 1st p.v.	-0.18	0.64	0.38	-0.03	-0.19	-0.21	-0.07	0.04	-0.32	0.19	0.14	82.90
a-p	-0.10	-0.17	-0.75	0.38	0.18	0.17	-0.01	-0.10	0.17	0.02	-0.15	86.71
m-l	0.01	-0.26	0.25	-0.45	0.08	-0.57	0.34	-0.12	0.17	-0.07	0.14	84.03
S—i	-0.33	0.19	0.37	-0.36	0.07	0.24	-0.43	0.20	-0.41^{*}	0.17	-0.06	90.45
Occlusal wear of UM1	-0.19	-0.08	0.48	0.07	0.35	-0.20	-0.28	-0.44	0.21	0.14	0.26	84.89
Total contribution (%)	12.31	11.49	10.06	9.45	8.04	7.03	6.49	5.67	4.86	4.27	3.84	83.50
Cumulative proportion (%)	12.31	23.80	33.86	43.32	51.35	58.38	64.87	70.55	75.40	79.67	83.50	83.50
¹ The sample size is 35. The nun	nber of prin	cipal comp	onents show	vn here wa	s determine	ed so that th	ne cumulati	ve proportic	on of the va	rriances of	the princips	l components
					1. 1:						- 1 7	
⁻ p.v.: principal value; a–p: direc	ction cosine	ior une ant	erior-poster	TOT AXIS; III		n cosine 10	r une meaia	I-lateral axi	s; s-1: alle	CUION COSIN	e ior the su	Derior-Interior

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axis. * P < 0.05; ** P < 0.01; *** P < 0.001, by a two-tailed bootstrap test.

Watadore Fac I II II IV V VI VII VII Node 3 (b) of Element 1: 1st p.v. -0.19 0.85^* -0.08 -0.02 0.008 -0.02 m-1 -0.02 -0.12 -0.03 0.012 -0.03 -0.02 -0.02 m-1 -0.02^* -0.111 0.88^{**} 0.011 -0.03 -0.044 -0.02 Node 4 (ba) of Element 1: 1st p.v. -0.111 0.88^{**} 0.011 -0.03 -0.044 -0.03 Node 4 (1) of Element 2: 1st p.v. -0.112 0.33 -0.144 0.002 -0.134 -0.032 Node 7 (ast) of Element 2: 1st p.v. -0.117 0.033 -0.12 -0.134 -0.032 -0.044 Node 7 (ast) of Element 2: 1st p.v. -0.117 0.033 -0.12 -0.134 -0.133 -0.144 -0.032 -0.164 Node 7 (ast) of Element 2: 1st p.v. -0.117 -0.135 -0.132 -0.164 -0.164 -0.164	Voriabla ²					H	actor loading	SS				
Node 3 (b) of Element 1: lst p.v. -0.19 0.85* -0.08 0.10 0.18 -0.11 0.02 0.04 -0.02 0.05 -0.02 0.05 -0.02 0.01 0.02 0.01 0.00 0.00 0.00 0.00 0.00	VALIAUIC	Fac I	Π	III	IV	٨	Ν	ΠΛ	VIII	IX	Х	IX
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	Node 3 (b) of Element 1: 1st p.v.	-0.19	0.85^{*}	-0.08	0.10	0.18	- 0.11	0.02	0.04	-0.02	-0.07	0.04
$ \begin{array}{cccccc} m-1 & -0.02 & 0.12 & -0.03 & 0.82^{***} & 0.10 & -0.06 & -0.08 & -0.06 \\ m-1 & 1.5tp.v. & 0.11 & 0.88 & -0.07 & 0.03 & 0.024 & 0.05 \\ m-1 & 0.52 & 0.29 & -0.03 & -0.01 & -0.03 & 0.024 & 0.05 \\ m-1 & 0.52 & 0.29 & -0.03 & -0.01 & 0.049 & 0.040 & -0.10 & -0.049 \\ m-1 & 0.52 & 0.29 & -0.03 & -0.04 & 0.001 & 0.49 & 0.040 & -0.19 \\ m-1 & 0.52 & 0.29 & -0.03 & -0.04 & 0.011 & 0.03 & 0.024 & 0.049 \\ m-1 & 0.01 & 0.03 & -0.04 & 0.01 & 0.049 & 0.011 & -0.049 \\ m-1 & 0.01 & 0.03 & -0.02 & -0.03 & 0.017 & -0.079^{***} & 0.016 & -0.049 \\ m-1 & 0.01 & 0.05 & 0.02 & 0.03 & 0.17 & -0.77^{***} & 0.23 & 0.04 \\ m-1 & 0.01 & 0.05 & 0.02 & -0.07 & 0.017 & -0.77^{***} & 0.23 & 0.04 \\ m-1 & 0.01 & 0.07 & -0.04 & 0.02 & 0.003 & 0.018 & -0.02 & 0.011 \\ m-1 & 0.01 & 0.07 & -0.04 & 0.01 & -0.05 & 0.00 & -0.044 & -0.10 \\ m-1 & 0.01 & 0.01 & -0.01 & -0.01 & 0.012 & 0.00 & 0.04 & -0.10 \\ m-1 & 0.01 & 0.01 & -0.01 & -0.01 & 0.01 & 0.017 & -0.07 & 0.010 & -0.02 \\ n-1 & 0.01 & 0.01 & -0.04 & 0.016 & 0.001 & -0.02 & 0.010 & 0.024 & -0.10 \\ n-1 & 0.01 & 0.01 & -0.04 & 0.016 & 0.012 & 0.011 & 0.02 & -0.01 \\ n-1 & 0.02 & 0.01 & -0.02 & -0.01 & 0.02 & -0.011 & 0.02 & 0.014 \\ m-1 & 0.08 & 0.06 & 0.01 & 0.01 & -0.04 & -0.10 & -0.02 & 0.01 & 0.024 & -0.10 \\ n-1 & 0.08 & -0.02 & 0.01 & 0.00 & -0.03 & 0.01 & 0.024 & -0.10 \\ n-1 & 0.08 & -0.02 & 0.01 & 0.00 & -0.04 & -0.10 & 0.02 \\ n-1 & 0.08 & -0.02 & 0.01 & 0.00 & -0.024 & 0.02 \\ n-1 & 0.08 & -0.02 & 0.01 & 0.00 & -0.04 & 0.01 & 0.00 & 0.018 & 0.024 & 0.01 & 0.024 \\ m-1 & 0.08 & -0.02 & 0.01 & 0.02 & -0.01 & 0.02 & 0.01 & 0.024 & 0.01 & 0.024 & 0.012 & 0.024 & 0.026 & 0.024 & 0.024 & 0.024 & 0.024 & 0.024 & 0.02$	a-p	0.83^{**}	-0.05	-0.13	-0.13	-0.12	-0.11	0.08	-0.02	0.17	0.12	0.11
Node 4 (ba) of Element 1: 1st p.v. 0.11 0.88* 0.07 0.11 -0.03 0.03 0.24 0.05 $^{-0.04}$ 0.07 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.09 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.00 $^{-0.04}$ 0.01 $^{-0.04}$ 0.01 0.04 $^{-0.04}$ 0.01 0.01 0.05 0.02 0.01 0.016 0.015 0.02 0.01 0.04 0.01 0.05 0.02 0.01 0.00 0.08 8.*** 0.113 0.04 0.01 0.02 0.01 0.012 0.01 0.017 0.017 0.015 0.013 0.012 0.012 0.017 0.017 0.015 0.013 0.013 0.017 0.00 0.018 0.05 0.014 0.010 0.01 0.01 0.01 0.01 0.017 0.017 0.010 0.012 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.012 0.012 0.012 0.010 0.010 0.010 0.010 0.010 0	m-l	-0.02	0.12	-0.03	0.82^{***}	0.10	-0.06	-0.08	-0.06	0.12	0.03	0.09
Node 4 (ba) of Element 1: 1st p.v. 0.11 0.88* 0.07 0.11 -0.03 -0.04 0.04 -0.04 0.092*** 0.25 0.29 -0.06 0.02 -0.10 0.01 0.49 0.40 -0.19 0.55 m_{m} -1 0.52 0.29 -0.03 0.092*** 0.13 0.23 0.049 0.01 0.49 0.40 -0.19 0.03 0.049 0.01 0.49 0.40 0.01 0.49 0.40 0.01 0.49 0.40 0.01 0.49 0.40 0.01 0.49 0.40 0.01 0.49 0.40 0.01 0.013 0.012 0.001 0.005 0.012 0.003 0.013 0.013 0.013 0.013 0.013 0.013 0.012 0.001 0.013 0.012 0.001 0.013 0.012 0.010 0.013	S-i	-0.92^{***}	-0.00	0.10	-0.13	-0.03	0.03	0.24	0.05	0.01	-0.01	-0.05
$ \begin{array}{llllllllllllllllllllllllllllllllllll$	Node 4 (ba) of Element 1: 1st p.v.	0.11	0.88^{*}	0.07	0.11	-0.03	-0.04	0.04	-0.04	-0.19	0.14	-0.00
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	a-p	-0.06	0.02	-0.10	-0.04	0.00	-0.10	-0.03	0.92^{***}	0.03	-0.02	-0.09
Node 4 (1) of Element 2: 1st p.v. -0.12 0.05 -0.20 -0.10 -0.15 -0.32 -0.16 -0.49^{*} $a - p$ 0.01 0.01 0.02 0.03 0.14 0.02 0.17 -0.51^{*} -0.23 0.09 $a - p$ 0.01 0.01 0.02 0.03 0.03 0.17 -0.7^{****} 0.23 0.09 $a - p$ 0.017 0.05 -0.03 0.02 0.003 0.17 -0.7^{****} 0.23 0.09 a - p 0.12 -0.05 -0.01 0.02 0.003 0.16 -0.27 0.11 0.09 $0.015a - p 0.12 0.01 0.012 0.00 0.08 0.8^{****} 0.12 0.01a - p$ 0.12 -0.01 0.07 -0.04 0.07 0.02 -0.017 0.02 -0.01 0.02 -0.010 $0.02a - p$ 0.12 -0.014 0.07 -0.04 0.07 0.02 -0.019 -0.02 -0.02 $-0.02Node 2 (fmt) of Element 2: 1st p.v. 0.17 0.069^{**} 0.02 -0.017 0.02 -0.019 -0.02 0.02a - p$ 0.012 -0.04 0.07 0.02 -0.017 0.02 -0.019 -0.02 $-0.02Node 2 (fmt) of Element 3: 1st p.v. -0.04 0.07 0.02 -0.02 0.02 -0.010 0.02 -0.011 0.02a - p$ -0.04 0.07 $0.02Node 5 (n) of Element 3: 1st p.v. -0.14 0.26 0.80^{***} 0.17 0.02 -0.02 -0.02 0.03 0.014 0.016 0.013 0.02 -0.012 0.02 -0.02 0.000 0.02a - p$ -0.010 0.02 0.00 0.02 -0.016 0.013 0.02 -0.016 0.013 0.02 -0.010 0.02 0.014 0.012 0.03 0.014 0.016 0.013 0.02 -0.010 0.02 0.014 0.012 0.02 0.000 0.013 0.02 0.014 0.012 0.02 -0.011 0.07 0.02 0.014 0.012 0.02 0.014 0.012 0.02 0.001 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02 0.012 0.02	m_l	0.52	0.29	-0.03	-0.09	0.01	0.49	0.40	-0.19	-0.15	0.10	0.10
Node 4 (1) of Element 2: 1st p.v. -0.12 0.38 0.14 0.44 0.02 0.17 $-0.51^* -0.23$ $a-p$ -0.14 0.03 0.03 0.17 -0.62^* 0.16 -0.06 -0.18 -0.14 $m-1$ 0.01 0.05 0.03 0.12 0.03 0.17 -0.71^{****} 0.23 0.09 0.04 $m-1$ 0.01 0.01 0.05 0.02 0.00 0.08 0.85^{****} 0.13 0.04 0.01 0.17 -0.27 0.11 0.04 0.04 0.01 0.01 0.017 -0.06 -0.16 -0.16 -0.27 0.11 0.01 0.012 0.04 0.01 0.017 0.017 0.009 -0.05 -0.00 -0.04 -0.02 0.014 -0.02 0.014 -0.02 0.00 -0.04 -0.02 0.014 -0.02 0.00 -0.04 -0.02 0.00 -0.04 -0.02 0.00 -0.04 -0.02 0.00 -0.04 -0.02 0.00 -0.04 -0.02 0.01 0.02 -0.01 -0.02 0.014 -0.02 0.014 -0.02 0.00 -0.04 -0.02 0.00 -0.04 -0.02 0.00 -0.04 -0.02 0.00 -0.04 -0.02 0.00 -0.04 -0.02 0.00 -0.02 0.014 -0.02 0.00 -0.02 -0.01 0.07 0.09 -0.02 0.014 -0.02 0.014 -0.23 0.012 0.02 -0.010 0.007 -0.012 0.02 -0.010 0.02 -0.011 0.02 -0.012 0.02 -0.011 0.02 -0.012 0.02 -0.012 0.02 -0.02 0.014 -0.02 0.02 -0.02 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.23 0.02 -0.02 -0.00 -0.011 0.02 -0.011 0.02 -0.011 0.02 -0.012 0.02 -0.012 0.02 -0.02 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.014 -0.22 0.012 -0.02 0.02 -0.012 0.02 -0.02 0.007 -0.02 0.007 -0.04 -0.012 0.02 -0.012 0.02 -0.012 0.02 -0.012 0.02 -0.02 0.000 -0.02 0.000 -0.02 0.000 -0.02 0.000 -0.014 0.012 0.02 -0.012 0.02 -0.02 0.000 -0.011 0.004 -0.018 -0.02 0.007 -0.02 0.007 -0.02 0.007 -0.02 0.007 -0.02 0.000 -0.02 0.000 -0.02 0.000 -0.011 0.000 -0.011 0.000 -0.011 0.000 -0.011 0.000 -0.011 0.000 -0.011 0.000 -0.011 0.000 -0.011 0.000 -0.011 0.000 -0.011 0.000 -0.011 0.000 -0.011 0.000 -0.011 0.000 -0.023 -0.023 0.000 -0.023 0.000 $-0.$	S-i	-0.59^{*}	-0.06	-0.20	-0.10	-0.15	-0.32	-0.16	-0.49^{*}	0.08	0.17	-0.03
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	Node 4 (1) of Element 2: 1st p.v.	-0.12	0.38	0.14	0.44	0.02	0.17	-0.51^{*}	-0.22	-0.12	-0.31	-0.11
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	a-p	-0.14	0.03	-0.26	-0.62^{*}	0.16	-0.06	-0.18	-0.14	0.37^{*}	-0.07	0.30
Node 7 (ast) of Element 2: 1st p.v. 0.17 0.69^* 0.02 -0.010 0.08 0.85^{***} 0.13 0.04 m^{-1} 0.01 0.01 0.07 -0.01 -0.05 0.16 -0.27 0.01 m^{-1} 0.01 0.07 -0.01 -0.02 -0.011 -0.02 -0.011 0.09 -0.02 -0.010 s^{-1} -0.27 -0.06 0.04 0.16 0.02 -0.011 0.29 -0.02 Node 2 (fmt) of Element 3: 1st p.v. 0.00 -0.06 0.04 0.16 0.02 -0.11 0.29 -0.02 m^{-1} 0.00 -0.04 -0.21 0.00 -0.04 0.07 0.21 0.83^{***} -0.19 -0.22 0.14 m^{-1} 0.08 0.06 0.00 -0.02 -0.02 -0.01 0.02 -0.01 0.07 0.19 m^{-1} 0.08 0.06 0.00 -0.02 -0.02 -0.00 -0.04 -0.02 0.00 -0.02 0.00 -0.02 -0.00 0.00 0.00 0.00 0.00 0.02 -0.00 -0.04 0.02 0.00 0.00 0.00 0.02 -0.01 0.02 0.00 0.00 0.02 -0.00 0.00 0.02 0.00	m_l	0.01	0.05	0.02	0.03	0.17	-0.77^{***}	0.23	0.09	-0.13	0.24	0.04
Node 7 (ast) of Element 2: 1st p.v. 0.17 0.69^* 0.02 -0.10 -0.05 0.16 -0.27 0.11 a-p 0.12 -0.01 0.07 -0.04 0.09 -0.05 -0.00 -0.04 $-0.10s-i$ -0.27 -0.01 0.07 -0.04 0.05 -0.00 -0.04 $-0.02Node 2 (fmt) of Element 3: 1st p.v. 0.00 -0.04 0.07 0.21 0.83^{***} -0.19 -0.22 0.14a-p$ -0.04 -0.36 -0.21 0.34 -0.33 -0.01 0.07 $0.12Node 5 (n) of Element 3: 1st p.v. -0.04 -0.36 -0.21 0.83^{***} -0.19 -0.22 0.14a-p$ -0.06 0.07 0.02 -0.02 -0.01 0.07 $0.01Node 5 (n) of Element 3: 1st p.v. -0.04 -0.26 0.00 -0.02 -0.02 -0.00 -0.084^{****} 0.12Node 5 (n) of Element 3: 1st p.v. -0.14 0.26 0.80^{****} 0.17 0.07 -0.06 0.07 0.02Node 5 (n) of Element 3: 1st p.v. -0.14 0.26 0.80^{****} 0.17 0.07 -0.01 0.07 -0.01 0.07 -0.01 0.02Node 5 (n) of Element 3: 1st p.v. -0.14 0.26 0.80^{****} 0.17 0.07 -0.06 0.07 0.02Node 5 (n) of Element 3: 1st p.v. -0.14 0.26 0.80^{****} 0.17 0.07 -0.01 0.07 -0.01 0.02 0.00 0.00 0.00 0.00 0.02 0.00$	S—i	-0.05	-0.03	0.12	0.00	0.08	0.85^{***}	0.13	0.04	-0.03	0.27	0.08
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Node 7 (ast) of Element 2: 1st p.v.	0.17	0.69^{*}	0.02	-0.10	-0.05	0.16	-0.27	0.11	0.10	-0.28	0.19
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	a-p	0.12	-0.01	-0.13	-0.07	0.17	0.09	-0.15	0.13	-0.26	0.77^{***}	-0.10
Node 2 (fmt) of Element 3: 1st p.v. $0.00 -0.04 0.07 0.21 0.83^{***} -0.19 0.22 0.14$ a-p -0.04 -0.36 -0.21 0.34 -0.33 -0.01 0.07 0.19 m-1 0.08 0.06 0.00 -0.02 -0.02 0.01 0.07 0.19 $m-1 0.08 0.06 0.17 0.22 -0.02 -0.02 -0.00 -0.84^{***} 0.02$ Node 5 (n) of Element 3: 1st p.v0.14 0.26 0.80^{***} 0.17 0.07 -0.06 0.07 0.08 $a-p -0.10 0.08 -0.74^{***} -0.19 0.00 -0.84^{***} 0.12$ m-1 0.08 -0.22 0.14 0.26 0.00 -0.02 -0.02 -0.01 0.07 0.08 $a-p -0.01 0.08 -0.74^{***} -0.09 0.00 -0.39 -0.01 0.04$ $m-1 0.08 -0.22 0.74^{***} -0.09 0.00 -0.39 -0.01 0.04$ $m-1 0.08 -0.22 0.74^{***} -0.09 0.00 -0.03 -0.01 0.02 0.01$ $s-i -0.23 -0.25 0.74^{***} -0.02 0.00 -0.01 0.06 -0.11 0.10 0.00$ s-i -0.01 -0.01 -0.08 0.16 0.12 -0.04 -0.02 0.12 -0.23 0.28 -0.004 -0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.0	m_l	0.01	0.07	-0.04	0.09	-0.05	-0.00	-0.04	-0.10	0.11	-0.16	0.92^{***}
Node 2 (fmt) of Element 3: 1st p.v. $0.00 -0.04 0.07 0.21 0.83^{***} -0.19 -0.22 0.14$ a-p -0.04 -0.36 -0.21 0.34 -0.33 -0.01 0.07 0.19 $m-1 0.08 0.06 0.17 0.20 -0.02 -0.02 -0.00 -0.84^{***} 0.02$ Node 5 (n) of Element 3: 1st p.v. $-0.14 0.26 0.00 -0.02 -0.16 0.83^{***} 0.13 0.29 -0.12$ $m-1 0.08 -0.74^{***} 0.17 0.07 -0.06 0.07 0.08$ $m-1 0.08 -0.74^{***} -0.19 0.00 -0.39 -0.01 0.04$ $m-1 0.08 -0.22 0.74^{***} -0.19 0.00 -0.39 -0.01 0.04$ $m-1 0.08 -0.22 0.74^{***} -0.09 0.00 -0.39 -0.01 0.04$ $m-1 0.08 -0.22 0.74^{***} -0.09 0.00 -0.39 -0.01 0.02$ $m-1 0.08 -0.23 0.74^{***} -0.02 0.00 -0.01 0.06 -0.11 0.06 -0.11 0.10$ m-1 -0.01 -0.01 -0.08 0.16 0.12 -0.04 -0.02 0.12 -0.23 m-1 0.10 -0.01 -0.08 0.16 0.12 -0.04 -0.02 0.12 -0.23 m-1 -0.01 -0.01 -0.08 m-16 metrior-posterior axis; m-1. direction cosine for the medial-lateral axis; s-i: direction	S-i	-0.27	-0.06	0.04	0.16	0.02	-0.11	0.29	-0.02	0.26	-0.10	-0.74^{***}
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Node 2 (fmt) of Element 3: 1st p.v.	0.00	-0.04	0.07	0.21	0.83^{***}	-0.19	-0.22	0.14	-0.02	-0.01	0.01
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	a-p	-0.04	-0.36	-0.21	0.34	-0.33	-0.01	0.07	0.19	-0.58^{**}	-0.12	0.18
Node 5 (n) of Element 3: 1st p.v. -0.06 0.17 0.02 -0.16 0.83*** 0.13 0.29 -0.12 Node 5 (n) of Element 3: 1st p.v. -0.14 0.26 0.80*** 0.17 0.07 -0.06 0.07 0.08 m ⁻¹ 0.08 -0.26 0.80*** 0.17 0.07 -0.06 0.07 0.04 m ⁻¹ 0.08 -0.22 0.02 -0.74 *** -0.09 0.00 -0.39 -0.01 0.04 S ⁻¹ -0.23 -0.25 0.74*** -0.23 0.07 -0.11 0.06 -0.11 0.10 -0.28 0.74*** -0.23 0.07 -0.11 0.06 -0.11 0.10 -0.28 0.74*** -0.23 0.07 -0.11 0.06 -0.11 0.10 $^{-1}$ The sample size is 35. The cumulative proportion of the variances of the eleven principal components is 83.50%.	m-l	0.08	0.06	0.00	-0.02	-0.02	-0.00	-0.84^{***}	0.02	0.15	0.08	0.26
Node 5 (n) of Element 3: 1st p.v. -0.14 0.26 0.80*** 0.17 0.07 -0.06 0.07 0.08 -0.74 *** 0.17 0.07 -0.06 0.07 0.08 -0.74 *** -0.09 0.00 -0.39 -0.01 0.04 -0.10 -0.14 -0.22 0.02 -0.74 *** -0.09 0.00 -0.39 -0.01 0.04 -0.28 0.04 -0.11 0.06 -0.11 0.10 -0.28 0.07 -0.11 0.10 -0.28 0.07 -0.11 0.06 -0.11 0.10 -0.28 0.06 -0.11 0.10 -0.28 0.07 -0.12 0.07 -0.12 -0.28 0.07 -0.28 0.00 -0.08 0.00 -0.28 0.00 $-$	S-i	-0.06	0.17	0.02	-0.16	0.83^{***}	0.13	0.29	-0.12	-0.02	0.14	-0.08
$\begin{array}{ccccc} a-p & -0.10 & 0.08 & -0.74^{***} & -0.09 & 0.00 & -0.39 & -0.01 & 0.04 \\ m-1 & 0.08 & -0.22 & 0.02 & 0.07 & -0.11 & 0.06 & -0.11 & 0.10 \\ s-i & -0.23 & -0.25 & 0.74^{***} & -0.23 & 0.08 & -0.06 & -0.18 & -0.28 \\ Occlusal wear of UM1 & -0.01 & -0.01 & 0.00 & 0.16 & 0.12 & -0.02 \\ \end{array} $	Node 5 (n) of Element 3: 1st p.v.	-0.14	0.26	0.80^{***}	0.17	0.07	-0.06	0.07	0.08	0.03	-0.00	-0.24
$ \begin{array}{ccccc} m-1 & 0.08 & -0.22 & 0.02 & 0.07 & -0.11 & 0.06 & -0.11 & 0.10 \\ s-i & -0.23 & -0.25 & 0.74^{***} & -0.23 & 0.08 & -0.06 & -0.18 & -0.28 \\ Occlusal wear of UM1 & -0.01 & -0.08 & 0.16 & 0.12 & -0.04 & -0.02 & 0.12 & -0.23 \\ \end{array} $	a-p	-0.10	0.08	-0.74^{***}	-0.09	0.00	-0.39	-0.01	0.04	-0.36^{*}	0.04	-0.08
S-i -0.23 -0.25 0.74^{***} -0.23 0.08 -0.06 -0.18 -0.28 Occlusal wear of UM1 -0.01 -0.01 -0.08 0.16 -0.18 -0.23 0.12 -0.23 ¹ The sample size is 35. The cumulative proportion of the variances of the eleven principal components is 83.50%. ² p.v.: principal value; a-p: direction cosine for the anterior-posterior axis, m-l: direction cosine for the medial-lateral axis; s-i: direction cosine for the medial component s axis; s-i: direction cosine for the medial component s axis; s-i: direction cosine for the medial component s axis; s-i: direction cosine for the medial component s axis; s-i: direction cosine for the medial component s axis; s-i: direction cosine for the medial component s axis; s-i: direction cosine for the medial component s axis; s-i: direction cosine for the medial component s axis; s-i: direction cosine for the medial component s axis; s-i: direction cosine for the medial component s axis; s-i: direction cosine for the medial component s axis; s-i: direction cosine for the medial component s axis; s-i: direction	m_l	0.08	-0.22	0.02	0.07	-0.11	0.06	-0.11	0.10	0.86^{***}	-0.01	0.01
$\begin{array}{cccc} \hline 0.12 & -0.04 & -0.02 & 0.12 & -0.23 \\ \hline 0.12 & -0.04 & -0.02 & 0.12 & -0.23 \\ \hline 0.12 & -0.23 & -0.23 & -1. \\ \hline 0.12 & -0.23 & -0.23 & -1. \\ \hline 0.12 & -0.23 & -1. \\ \hline 0.12 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.23 & -1. \\ \hline 0.12 & -0.22 & -0.22 & -0.22 & -0.22 & -0.22 & -0.22 & -0.23 & -$	S-i	-0.23	-0.25	0.74^{***}	-0.23	0.08	-0.06	-0.18	-0.28	-0.23	0.07	0.10
¹ The sample size is 35. The cumulative proportion of the variances of the eleven principal components is 83.50%. ² p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction	Occlusal wear of UM1	-0.01	-0.08	0.16	0.12	-0.04	-0.02	0.12	-0.23	0.33	0.79^{***}	-0.02
² p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction	¹ The sample size is 35. The cu	mulative prop	ortion of the	variances of 1	the eleven p	rincipal com	ponents is 83	3.50%.				
	² p.v.: principal value; a–p: direc	ction cosine fo	r the anterio	r-posterior axis	s; m-l: direc	tion cosine fo	or the medial	-lateral axis;	s-i: direction	cosine for th	ne superior-in	ferior axis.
$^{*}P < 0.05$; $^{**}P < 0.01$; $^{***}P < 0.001$, by a two-tailed bootstrap test.	*P < 0.05; $**P < 0.01$; $***P < 0.01$; $**P < 0.01$;	< 0.001. bv a t	vo-tailed bo	otstrap test.							4	

Rotated solution of the first eleven principal components extracted from the correlations between the linearized first principal values and their direction

Vallaute					Factor	loadings					Total
	PC I	Π	III	IV	>	ΙΛ	ΠΛ	VIII	IX	Х	variance (%)
Node 3 (b) of Element 1: 1st p.v. 0.	.72***	0.12	0.07	0.17**	-0.14^{*}	0.10	0.04	0.27***	0.17***	0.02	69.78
a–p – 0.	.24	0.11	-0.47	0.18	0.41	-0.04	-0.00	-0.08	-0.36	0.47^{*}	84.85
m-1 -0 .	.08	0.45	0.12	-0.42	-0.12	-0.46	-0.16	-0.14	0.44^{**}	0.05	87.58
s-i 0.	.02	- 0.66	0.30	0.16	-0.19	0.17	0.21	-0.10	0.00	-0.03	67.87
Node 4 (ba) of Element 1: 1st p.v. 0.	$.60^{**}$	0.09	-0.19^{***}	0.50^{***}	0.03	0.13^{*}	0.24^{***}	0.25^{***}	0.06	-0.10^{*}	81.36
a–p 0.	.29	0.26	-0.33	0.07	0.63^{*}	-0.28	-0.26	0.10	0.05	-0.20	86.02
m–l – 0.	.10	0.32	0.65	0.13	-0.13	-0.45^{**}	0.24	-0.12	-0.07	0.02	85.77
s-i -0.	-27	-0.39	-0.04	-0.63^{*}	0.12	0.22	-0.04	0.10	0.21	0.32^{*}	84.92
Node 4 (1) of Element 2: 1st p.v. 0.	.55*	0.12^{*}	0.02	0.18^{***}	-0.05	-0.28^{***}	-0.26^{***}	-0.12^{**}	-0.16^{***}	0.52^{***}	81.56
a-p - 0.	.72***	-0.04	-0.19	0.19	0.49	0.12	-0.07	-0.06	0.12	0.01	86.94
m_1 0.	.14	0.64	0.46	-0.07	0.07	-0.17	0.00	0.26	-0.13	-0.00	76.10
s-i 0.	.12	- 0.47	-0.46	-0.49	-0.28	-0.17	-0.08	0.18	0.04	-0.03	84.33
Node 7 (ast) of Element 2: 1st p.v. 0.		- 0.50***	0.11	0.23^{***}	0.07	-0.40^{**}	0.20^{***}	-0.17^{**}	0.05	0.29^{***}	89.88
a–p 0.	.45*	0.09	0.29	-0.30	-0.33	0.30	-0.47^{*}	-0.00	-0.34	0.03	91.99
m-1 0.	.30 -	-0.11	-0.55^{**}	-0.21	0.04	-0.45^{**}	0.48^{*}	-0.09	0.12	-0.09	92.75
s-i -0.	.59**	-0.04	0.43	0.50	0.07	0.08	0.01	-0.03	0.25^{*}	0.02	85.51
Node 2 (fmt) of Element 3: 1st p.v. 0.	.46	0.08	0.17^{**}	0.01	0.17^{**}	0.37^{***}	0.22^{***}	0.27^{***}	0.44^{***}	0.21^{***}	77.77
a–p 0.	- 11.	- 0.46	0.06	0.37	0.12	-0.21	-0.42	-0.35	0.06	-0.29	80.34
m_l - 0.	$.60^{***}$	0.03	-0.09	0.11	-0.15	-0.14	0.37	0.53^{**}	-0.30^{*}	0.09	93.60
s-i 0.	.25	0.60	-0.18	0.01	0.12	0.42	0.15	-0.42^{*}	0.17	0.13	88.81
Node 5 (n) of Element 3: 1st p.v. 0.	.12	0.47^{**}	-0.46^{**}	0.03	-0.32^{*}	0.10	0.24^{*}	-0.18	-0.17	-0.28^{**}	75.15
a–p 0.	.52**	-0.57	0.21	-0.01	0.25	0.10	0.21	-0.08	-0.20	-0.07	79.79
m_l 0.	.02	-0.06	0.56	-0.44	0.49	-0.17	0.21	0.16	-0.10	-0.13	88.33
si -0.	- 33	- 0.08	-0.18	0.40	-0.61^{*}	-0.20	-0.15	0.17	0.24	0.15	83.95
Age 0.	.25 -	- 0.09	-0.14	0.21	0.20	-0.10	-0.41	0.59^{**}	0.06	-0.08	70.40
Total contribution (%) 15.	.89	12.21	10.55	8.96	8.04	6.74	6.18	5.87	4.45	4.13	83.01
Cumulative proportion (%) 15.	.89	28.10	38.64	47.60	55.64	62.38	68.56	74.44	78.89	83.01	83.01

Princinal commonent analysis of the correlations between the linearized first nrincinal values and their direction cosines at six craniofacial landmarks i e Table 22 27

² p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction cosine for the superior-inferior

* P < 0.05; ** P < 0.01; *** P < 0.001, by a two-tailed bootstrap test.

axis.

Three-Dimensional Structural Deviations at Cranial Landmarks

at six craniotacial landmarks,	1.e., b, ba, l, a:	st, tmt, and n 1	n the three ri	ght elements,	and age in Air	Ican-America	US.			
Voriable ²					Factor]	oadings				
VallaUIC	Fac I	Π	III	IV	Λ	Ν	ΠΛ	VIII	IX	Х
Node 3 (b) of Element 1: 1st p.v.	0.35	- 0.07	0.07	0.67*	-0.04	- 0.12	- 0.08	0.17	- 0.25	0.00
a-p	-0.31^{*}	0.16	-0.28	-0.20	0.06	0.02	0.20	-0.03	-0.04	0.75^{***}
m-l	0.03	0.59^{*}	0.53	-0.03	-0.11	-0.23	-0.24	-0.10	0.31	-0.12
S—i	-0.00	-0.77^{***}	-0.04	0.01	-0.09	0.09	-0.04	-0.08	0.11	-0.21
Node 4 (ba) of Element 1: 1st p.v.	0.00	-0.15	-0.13	0.62^{*}	-0.03	-0.12	0.01	0.17	-0.58^{**}	0.09
a-p	-0.21	0.43^{**}	-0.09	0.09	0.37	-0.20	-0.33	0.45^{**}	-0.25	0.24
m-I	-0.02	-0.05	0.87^{*}	-0.10	0.03	0.17	0.08	-0.15	-0.14	-0.02
S-i	-0.03	-0.03	-0.27	-0.03	0.12	-0.09	0.12	-0.07	0.85^{***}	-0.07
Node 4 (1) of Element 2: 1st p.v.	0.39	-0.03	0.24	0.21	-0.13	-0.09	-0.26	0.10	-0.08	0.68^{***}
a-p	-0.72^{***}	0.18	-0.28	-0.29	0.04	0.35	0.03	0.03	0.16	0.07
m	0.24	0.38	0.57	0.17	0.28	0.22	0.20	0.10	-0.16	0.02
S-i	0.23	-0.09	-0.32	-0.15	-0.18	-0.66^{**}	0.05	0.21	0.35	-0.15
Node 7 (ast) of Element 2: 1st p.v.	-0.02	-0.64^{**}	0.26	0.22	-0.02	-0.35	-0.31	0.10	0.01	0.36^{*}
a-p	0.92^{***}	0.03	-0.06	0.02	0.10	0.20	-0.11	0.01	0.05	-0.02
m-l	-0.22	-0.02	-0.01	0.07	0.06	-0.92^{***}	-0.01	-0.08	-0.12	0.06
S-i	-0.52^{***}	-0.16	0.24	-0.07	-0.24	0.65^{***}	0.01	-0.02	0.05	-0.14
Node 2 (fmt) of Element 3: 1st p.v.	0.01	-0.03	-0.02	0.85^{***}	0.15	0.07	-0.00	-0.01	0.13	-0.04
a-p	-0.09	-0.36	-0.05	-0.28	-0.08	0.08	-0.69^{***}	0.28	-0.15	-0.01
m-l	-0.30	-0.02	0.09	-0.25	-0.19	0.04	0.85^{***}	0.16	-0.03	-0.01
S-i	0.02	0.42^{*}	-0.15	0.40^{*}	0.13	0.08	-0.19	-0.62^{***}	-0.23	0.17
Node 5 (n) of Element 3: 1 st p.v.	0.13	0.33	-0.18	-0.02	-0.12	-0.29	0.15	-0.38	-0.57^{**}	-0.09
a-p	0.15	-0.69^{***}	-0.10	0.18	0.44	-0.15	-0.18	0.07	-0.03	0.05
m-l	-0.04	-0.10	0.40	-0.01	0.75***	0.02	0.10	0.14	0.29	-0.17
Si	-0.10	-0.02	0.07	-0.09	-0.88^{***}	0.04	0.12	0.14	-0.01	-0.05
Age	0.06	0.09	- 0.16	0.23	- 0.03	0.02	- 0.04	0.78***	- 0.07	0.06
¹ The sample size is 27. The curr ² p.v.: principal value; a–p: directi	ulative propor ion cosine for t	tion of the var he anterior-pos	iances of the sterior axis; r	e ten principal n-l: direction e	components is cosine for the r	83.01%. nedial-lateral	txis; s–i: direct	tion cosine for	r the superior-i	nferior axis.
*P < 0.05; **P < 0.01; ***P < 0.01	0.001, by a two	o-tailed bootst	rap test.							

Rotated solution of the first ten principal components extracted from the correlations between the linearized first principal values and their direction cosines

Table 23.

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ValuationPC IIIIIIINode 3 (b) of Element 1: 1st p.v. 0.67^{**} 0.15^{**} $0.1.$ $a-p$ 0.19 -0.48 0.1 $m-1$ 0.06 0.04 0.1 $n-1$ 0.06 0.72 -0.33 Node 4 (ba) of Element 1: 1st p.v. 0.78^{***} 0.08 0.22 $m-1$ 0.35 -0.02 -0.02 $m-1$ 0.35 -0.26 0.16 $n-1$ 0.35 -0.36 -0.54 Node 4 (l) of Element 2: 1st p.v. 0.48 -0.05 0.3	III IV 14* -0.22* 18 0.16 13 -0.28 32*** 0.13*	Λ					Total
Node 3 (b) of Element 1: 1st p.v. 0.67^{**} 0.15^{*} 0.1 a^{-p} 0.0 0.19 -0.48 0.1 m^{-1} 0.06 0.04 0.1 s^{-i} -0.09 0.72 -0.3 Node 4 (ba) of Element 1: 1st p.v. 0.78^{***} 0.08 0.2 m^{-1} 0.35 -0.02 -0.05 m^{-1} 0.36 0.54 0.1 Node 4 (1) of Element 2: 1st p.v. 0.48 -0.05 0.3	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	•	ΙΛ	ΠΛ	VIII	IX	variance (%)
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	118 0.16 13 -0.28 32 0.06 222*** 0.13*	** 0.12*	0.07	-0.15^{**}	0.17**	0.52***	88.04
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-0.50^{*}	-0.00	0.09	-0.38	-0.23	77.57
	32 0.06 22*** 0.13*	0.03	0.61^{*}	-0.28	-0.49^{*}	0.31	88.40
Node 4 (ba) of Element 1: 1st p.v. 0.78*** 0.08 0.2: a-p 0.16 -0.02 -0.0 m-l 0.35 -0.36 -0.5 s-i -0.38 0.54 0.1 Node 4 (l) of Element 2: 1st p.v. 0.48 -0.05 0.3	22*** 0.13*	0.17	0.11	0.20	0.25	-0.17	80.26
$ \begin{array}{ccccc} a-p & 0.16 & -0.02 & -0.0 \\ m-l & 0.35 & -0.36 & -0.5 \\ s-i & -0.38 & 0.54 & 0.1 \\ Node 4 \ (l) \ of Element 2: 1 st p.v. & 0.48 & -0.05 & 0.3 \\ \end{array} $		0.01	0.27^{***}	-0.06	0.19^{***}	-0.25^{***}	85.50
$ \begin{array}{ccccc} m-i & 0.35 & -0.36 & -0.5' \\ s-i & -0.38 & 0.54 & 0.1 \\ \text{Node 4 (1) of Element 2: 1st p.v.} & 0.48 & -0.05 & 0.3 \\ \end{array} $	$01 0.76^{\circ}$	-0.10	-0.00	0.03	-0.44^{*}	0.15	83.05
s-i -0.38 0.54 0.1 Node 4 (1) of Element 2: 1st p.v. 0.48 -0.05 0.3	50 - 0.21	-0.17	0.22	0.29	0.14	-0.30	80.82
Node 4 (1) of Element 2: 1st p.v. 0.48 – 0.05 0.3	$17 - 0.55^*$	0.18	0.04	0.14	0.07	-0.07	83.09
	33*** 0.25*	** 0.51***	0.05	-0.43^{***}	0.05	-0.13^{*}	86.96
a-p -0.31 -0.05 0.1	$11 0.74^*$	0.34	-0.01	0.16	0.19	-0.04	83.85
m-1 -0.15 0.15 -0.0	05 - 0.19	-0.45	0.53	0.32	0.05	0.29	75.11
s-i 0.14 -0.32 0.1	17 - 0.52	-0.20	-0.57^{**}	0.17	-0.21	-0.06	87.04
Node 7 (ast) of Element 2: 1st p.v. $0.64^* - 0.45^{**} - 0.0$	$04 - 0.28^{*}$	* 0.27***	0.35^{***}	0.01	0.20^{*}	-0.12	93.08
a-p 0.17 0.5	$58^* - 0.23$	0.17	-0.04	0.23	-0.06	-0.36	66.07
m-1 0.42* 0.18 -0.4	48 0.28	0.19	0.04	0.48^{*}	0.00	0.17	81.28
$s-i = -0.72^{***} 0.21 0.2$	22 0.09	-0.11	0.12	-0.44^{*}	0.12	-0.01	85.68
Node 2 (fmt) of Element 3: 1st p.v. 0.47 0.47*** 0.1	17^{**} 0.01	-0.16^{**}	-0.01	-0.23^{***}	-0.32^{***}	-0.31^{***}	74.90
$a-p - 0.44^* - 0.08 0.0$	06 - 0.28	0.45	0.18	-0.05	-0.16	-0.24	59.49
m_l 0.23 0.53 -0.4	45 - 0.25	0.20	-0.14	-0.08	-0.40^{**}	0.12	83.64
s–i 0.09 – 0.31 0.6	61 0.01	-0.34	-0.01	-0.01	0.45^{*}	0.27	87.21
Node 5 (n) of Element 3: 1st p.v. 0.11 0.58*** 0.2	24* 0.13	-0.44^{***}	0.15	0.04	0.04	-0.26^{**}	70.59
a-p -0.21 -0.73 -0.1	17 - 0.30	0.28	-0.01	-0.07	-0.02	0.00	77.44
m–l – 0.23 0.09 0.6	60 - 0.05	0.11	0.30	0.48^{*}	-0.15	0.00	78.09
s-i 0.19 0.42 -0.2	-0.23	-0.38	-0.23	-0.34	0.29	-0.04	74.23
Age 0.32 0.33 0.4	$49^* - 0.08$	0.24	-0.45	0.30	-0.05	0.31^{*}	90.94
Total contribution (%) 14.46 13.63 10.5	54 10.14	7.97	6.73	6.31	5.89	5.21	80.89
Cumulative proportion (%) 14.46 28.09 38.6	64 48.78	56.75	63.49	69.79	75.68	80.89	80.89
¹ The sample size is 27. The number of principal components show	wn here was dete	rmined so that the	e cumulative	proportion of	the variances	of the princip	al component
exceeded 80%. ² n v. minoinal value: a_n. direction cosine for the anterior-mosteri.	rior avis: m_l· dir	action cosine for	the medial-la	itaral avie e	i. direction co	oine for the ci	nerior-inferi
² p.v.: principal value; a-p: direction cosine for the anterior-posteri	rior axis; m-l: dir	ection cosine for	the medial-la	ateral axis; s-	i: direction co	sine for the su	perio

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axis. * P < 0.05; ** P < 0.01; *** P < 0.001, by a two-tailed bootstrap test.

Vouinhla2				Fa	ctor loadings				
Vallaure	Fac I	Π	Ш	IV	Λ	IV	VII	VIII	IX
Node 3 (b) of Element 1: 1st p.v.	0.16	0.05	-0.24	-0.08	-0.09	0.39	0.30	0.12	0.72***
a-p	-0.06	-0.49	0.13	0.56^{*}	-0.12	0.06	0.18	0.25	-0.30
m_l	-0.05	0.03	0.15	0.02	0.00	0.92^{***}	-0.02	-0.10	-0.00
S-i	-0.16	0.50	-0.03	-0.36	-0.36	-0.26	-0.00	-0.44^{*}	0.04
Node 4 (ba) of Element 1: 1st p.v.	0.39	0.12	0.01	0.09	-0.49	0.11	0.60^{*}	0.19	0.16
a-p	0.07	0.17	0.09	0.86^{**}	-0.14	0.00	-0.13	-0.14	0.05
m_l	-0.24	-0.12	-0.16	0.01	0.09	-0.10	0.78^{***}	-0.07	-0.28
Si	-0.18	-0.00	0.27	-0.76^{**}	-0.16	0.06	-0.27	-0.21	0.08
Node 4 (1) of Element 2: 1st p.v.	0.85^{***}	0.20	0.05	0.09	-0.08	0.15	0.16	0.11	0.17
a-p	0.18	0.56^{*}	0.31	0.31	0.15	-0.46^{*}	-0.24	0.11	-0.07
m_l	-0.74^{***}	0.16	0.08	-0.08	-0.16	0.32	0.09	0.15	-0.01
S—i	-0.03	-0.89^{***}	0.01	-0.10	0.15	-0.13	0.06	0.04	0.16
Node 7 (ast) of Element 2: 1st p.v.	0.30	-0.02	0.01	-0.10	0.19	0.24	0.84^{***}	0.17	0.05
a-p	0.26	-0.26	0.53^{*}	-0.29	-0.34	-0.06	0.09	0.07	0.13
m-l	-0.19	0.33	-0.02	0.28	-0.01	-0.23	0.46^{**}	-0.45^{*}	0.35
S-i	-0.02	0.26	-0.05	-0.24	-0.05	0.12	-0.72^{***}	0.24	-0.36^{*}
Node 2 (fmt) of Element 3: 1st p.v.	0.31	-0.19	-0.05	0.08	-0.71^{**}	0.21	0.04	-0.24	0.04
a-p	0.16	0.03	0.37	-0.38	0.31	0.14	-0.14	-0.19	-0.33
m-l	0.00	-0.05	-0.24	-0.11	-0.13	0.20	-0.01	-0.80^{***}	0.26
S-i	-0.04	-0.11	0.02	0.01	-0.03	0.00	-0.01	0.89^{***}	0.26
Node 5 (n) of Element 3: 1st p.v.	-0.14	0.08	0.04	-0.04	-0.82^{***}	-0.01	-0.08	0.07	-0.04
a-p	0.09	-0.22	0.02	-0.10	0.77^{***}	0.07	0.17	0.08	-0.27^{*}
m_l	-0.19	0.03	0.81^{***}	-0.11	-0.12	0.10	-0.11	0.17	0.09
s-i	-0.08	-0.08	-0.69^{***}	-0.28	-0.40^{*}	-0.06	-0.02	-0.06	0.07
Age	0.16	-0.22	0.29	-0.06	-0.17	-0.16	-0.13	-0.05	0.82^{***}

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Tabl	e 26. Kendall's rank and rotated factors obt	correlation tained fron	n coefficient n the first set	s between t t of neuroci	the right a ranial lan	and left side dmarks (ft,	es of three STH, i, SC	samples in CH, g, and	the varia zm) and c	tion patter lental wea	n of factor r or age. ¹	· loadings o	on the prine	cipal com	onents
				-	5	ε	4	5	9	2	×	6	10	=	12
- 0	Japanese	Right	PC IV Fac VIII	35*											
ŝ		Left	PC VIII			-									
4	;		Fac VIII			.51***) 								
ŝ	Indians	Right	PCI				.38**								
9		,	FacIX												
2		Left	PC III												
×			Fac IV	.35*				.42**							
6	A frican-Americans	Right	PC II												
10			Fac II					.32*			.31*	.51***			
11		Left	PC VII	.31*											
12			Fac IX									.45**	.53***		
Tabl	P<0.05; ** P<0.01; * e 27. Kendall's rank and rotated factors obt	P < 0.0 correlation tained from	001, by a two n coefficient n the second	-tailed test s between t set of neur	the right a rocranial	and left side landmarks	es of three (b, ba, l, a	samples in st, fmt, and	the varia n th varia	tion patter ental wear	m of factor or age. ¹	· loadings o	on the prine	cipal com	onents
				1	2	3	4	5	9	7	8	6	10	11	12
-	Japanese	Right	PC IV												
0	4)	Fac IV	.53***											
ŝ		Left	PC VIII												
4			Fac VIII												
S	Indians	Right	PCV												
9			Fac VI					.32*							
2		Left	PC III						.37*						
8			Fac X			.28*				.28*					
6	African-Americans	Right	PC VIII	.33*							.29*				
10			Fac VIII	.						.		.46**			
11		Left	PC III	.35*					.42**	.32*					
12			Fac IX	$.30^{*}$.30*			

ur or age in each analysis were compared with one another.	befficients are removed because the signs of factor loadings	
¹ The principal components and rotated factors that were superficially most highly correlated with dental wee	Only those rank correlation coefficients significant at the 5% level are listed here. The signs of rank correlation co	are reversible. The original factor loadings are listed in Tables 14 to 25.

P*<0.05; *P*<0.01; ****P*<0.001, by a two-tailed test.

Light ← DENTAL WEAR → Heavy Weak ← STRAIN AT INION → Strong

O

perpendicular from bregma to the line segment, nasion-lambda. Each of these crania is one of the five lowest or five highest extremes in the scores of the PCs which Fig. 2. Two crania of early modern Japanese males, Nos. 10013 and 10078, superimposed in the original coordinate system, where the origin is set at the foot of the borhood of the landmarks analyzed is reliable because far regions off the landmarks are manually deformed from a template with Rokkaku-Daiou Super 6, a. No. are significantly correlated with both the degree of occlusal wear on the UM1 and the first principal value at the inion (Tables 2 and 4). Only the form in the neigh-10013 (left) and No. 10078 (right). b. Anterior view of superimposed crania. c. Posterior view. d. Lateral view from the right. e. Lateral view from the left. f. Superior view. g. Inferior view.



C

q

Variabla ²	Factor le	oadings
variable	PC III from right elemens	PC VI from left elements
Node 4 (ba) of Element 1: 1st p.v.	0.08	0.06
a-p	-0.30	0.06
m—l	0.77**	0.09
s—i	-0.32	-0.02
Node 2 (ba) of Element 2: 1st p.v.	0.01	-0.20^{***}
a-p	-0.18	-0.25
m–l	0.40	-0.00
s—i	0.17	0.49
Node 8 (ba) of Element 3: 1st p.v.	-0.32^{**}	0.03
a-p	0.18	-0.10
m–l	0.26	0.47
s—i	0.07	-0.02
Occlusal wear of UM1	-0.59^{***}	0.64***

Table 28. Principal components from two correlation matrices on the linearized first principal values and their direction cosines at basion and the degree of occlusal wear on the maxillary first molar.¹

¹ The sample consists of 33 skulls of early modern Japanese males (the first data set). The two PCs shown here were extracted from two correlation matrices on only two landmarks, basion and porion, for the right and left sides, respectively. Each of basion and porion is one of the eight nodes of each of three elements on either side of the skull. Both PCs are most highly correlated with dental wear among the PCs obtained from the respective correlation matrices.

² p.v.: principal value; a-p: direction cosine for the anterior-posterior axis; m-l: direction cosine for the medial-lateral axis; s-i: direction cosine for the superior-inferior axis.

*P < 0.05; **P < 0.01; ***P < 0.001, by a two-tailed bootstrap test.

broader facial region (Fig. 1). The remarkable findings, particularly from the viewpoint of repeatability between the results on the right and left sides, are 1) a significant positive association between the degree of dental wear and the magnitude of strain at the inion in Japanese (Tables 2 and 4; Fig. 2); 2) a significant inverse association between the degree of dental wear and the magnitude of strain at the frontotemporale in Japanese (Tables 2 and 4); 3) a significant positive association between age and the magnitude of strain at the center of the parietal tuber in African-Americans (Tables 11 and 13); and 4) significant positive and inverse associations of the degree of dental wear with the magnitude of strain at the frontomalare temporale and asterion, respectively, in Japanese (Tables 14 and 16).

As stated above, the details indicated by previous and the present FESAs of the same Japanese sample are not necessarily consistent. Besides, the results from the three samples examined here did not necessarily show similar tendencies at least regarding the associations with dental wear or age. Although the latter discrepancies are due possibly to some between-population differences in genetic and environmental factors, the former is considered to be caused, in part, by the approach to selecting landmarks in constructing an element or hexahedron in the skull. Namely, a landmark common to some different elements may show different tendencies in its principal value and direction cosines according to the elements selected. In Table 28, patterns of variation in factor loadings are shown for the 3D strain variables at a landmark, the basion, in six different elements. These patterns of variation reveal no clear consistency between different elements. Comparing with Tables 14 and 16, however, it can be found that the patterns of variation in factor loadings for Node 4 (ba) of Element 1 of both sides (PC IV in Table 14 and PC VIII in Table 16) are very similar to those (right PC III and left PC VI) shown in Table 28, even though the combination of variables to be used in PCAs differs. This suggests that 3D strain properties of each cranial local region are specific. In sum, when we obtain some information on a landmark by FESM, we should interpret it while keeping in mind the whole structure of the element to which the landmark in question belongs.

Interpreting the results of the present study in such a way, the following inferences may be pos-

sible.

1) If the degree of dental wear is merely an indicator of age, PC IV in Table 2 and PC VIII in Table 4 imply that the magnitude of strain in the neighborhood of the inion increases with age in Japanese. This may indicate greater variation in the development of the nuchal muscles in older people. Alternatively, if the degree of dental wear is due mainly to the extent of occlusal force and if the masticatory and nuchal muscles are considerably controlled by common genetic and/or environmental factors, it may be inferred that people with powerful skeletal muscles tend to have greater structural variation around the posterior end of the nuchal plane. At least, this finding is not considered an artificial phenomenon because the intra-observer errors for the principal value at the inion are fairly low (Table 1). Zafar et al. (2000) suggested on the basis of physiological experiments that functional jaw movements comprise concomitant mandibular and head-neck movements involving the temporomandibular, the atlanto-occipital, and the cervical spine joints, and are caused by jointly activated jaw and neck muscles. If so, the strong association between the inion and dental wear found in the present study may also partly be explained by this combination of mandibular and head-neck movements.

2) Similarly, both PC VIIIs in Tables 2 and 4 suggest that the magnitude of strain in the neighborhood of the frontotemporale decreases with age in Japanese, or tends to be smaller in individuals with stronger masticatory force. In any case, this phenomenon seems to be associated with the development of the temporalis muscle. As the intra-observer errors for the principal value at the frontotemporale are relatively low (Table 1), this finding seems reliable.

3) Fac II in Table 11 and Fac IX in Table 13 clearly show that the magnitude of strain at the center of the parietal tuber (SCH) increases with age in African-Americans. As the intra-observer errors for the principal value at SCH are relatively low (Table 1), this finding seems to be a biological phenomenon associated with aging. As

shown in Table 11, however, age is not only positively associated with the principal value at SCH but also inversely related with its direction cosine for the medial-lateral axis. If this is correct, it means that the center of the right parietal tuber tends to shift to the right side or laterally with age. However, the intra-observer errors in the direction cosine for the medial-lateral axis at SCH are very high (Table 1), and, furthermore, in the left parietal tuber, there is no similar tendency (Table 13). Therefore, it may be safe to say that, at least, the magnitude of strain at the center of the parietal tuber increases with age regardless of the direction. Mizoguchi (1992), using another sample from early modern Japanese males, suggested that individuals with heavier dental wear have smaller inter-parietaltuber breadth, smaller basibregmatic height, and greater bizygomatic breadth. The finding on SCH in the present study is not necessarily inconsistent with this suggestion by Mizoguchi (1992). Finally, it should be furthermore considered that the rate of admixture with other populations may be different from generation to generation in the United States. If so, this may also influence the association between the magnitude of strain at SCH and age.

4) PC IV in Table 14 and PC VIII in Table 16 imply that the magnitude of strain at the frontomalare temporale increases with age and, simultaneously, the magnitude of strain at the asterion decreases with age in Japanese, or the magnitude of strain tends to be larger at the frontomalare temporale and smaller at the asterion in individuals with stronger masticatory force. However, while the intra-observer error in the principal value at the right asterion is relatively low, those for the left asterion and the right and left frontomalare temporale are very high (Table 1). Therefore, it is difficult from these findings to make any meaningful argument.

Finally, from the present and previous findings, it can be said at least that the craniofacial form varies along with age even in adulthood and, possibly, also in response to mechanical stresses from the masticatory and/or nuchal muscles.

Interrelationship between 3D structural strains

In the above section, the focus of attention was the association between 3D structural strain and dental wear or age. Apart from this, however, the results of the present analyses further suggest some other strong associations in the magnitude of strain between several cranial landmarks across the three samples. For example, strong associations between the principal values at the bregma, basion, and lambda are indicated by two PC IIs from Japanese (Tables 14 and 16), Fac III from Indians (Table 19), and PC I from African-Americans (Table 22). In addition to these, Fac IIs from Japanese (Table 15) and Indians (Table 21), and Fac IV (Table 23) and PC I (Table 24) from African-Americans also show the strong association between the bregma and basion. Although the causes of these strong associations cannot be determined here because there are no data on candidate factors, one of the possible causes is the structural variation in height of the brain.

To determine the causes of such interrelationships between sub-structures of the skull, we should make every effort to collect a range of information on environmental factors together with skeletal materials.

Summary and Conclusions

In order to explore the possibility that the masticatory force and/or aging are causes of part of the morphological variation in the human skull, finite element scaling analysis (FESA) was carried out using three male adult samples from early modern Japanese, Indians, and African-Americans. Principal component analyses and the rotated solutions of the 3D structural deviations obtained by FESAs suggested that the magnitude of strain in the neighborhood of the inion increases with age in Japanese, or that people with powerful skeletal muscles tend to have greater structural variation around the posterior end of the nuchal plane; and that the magnitude of strain in the neighborhood of the frontotemporale decreases with age in Japanese, or tends to

be smaller in individuals with stronger masticatory force. It was clearly shown that the magnitude of strain at the center of the parietal tuber increases with age in African-Americans. In addition to these findings, strong associations in the magnitude of strain were also found between several landmarks such as bregma, basion, and lambda across the three samples.

At present, it can be said at least that the craniofacial form varies along with age even in adulthood and, possibly, also in response to mechanical stresses from the masticatory and/or nuchal muscles. In the future, data on other possible causes than dental wear, age, sex, and so on should also be collected.

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